

**LsDyna3D Simulations and Analysis of
Polish Governmental Airplane TU-154M
Crash in Smolensk, Russia, April 10, 2010**



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- **MS – Warsaw Polytechnic, SiMR**
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- **Director “UA Gas Turbine Facility”**
 - **Impact Laboratory**
 - **Structural Laboratory**
 - **Material Testing Laboratory**
- **www.ecgf.uakron.edu/~civil/people/binienda/**
- **www.uakroncivil.com/researchlab/**

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- Arizona State University (ASU)
- Boeing
- Central Connecticut State University (CCSU)
- Federal Aviation Administration (FAA)
- General Electric Aviation (GE)
- George Washington University (GWU)
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- Hamilton Sundstrand
- Honeywell
- LSTC
- National Aeronautics and Space Administration (NASA)
- Ohio State University (OSU)
- Pratt & Whitney
- Rolls-Royce
- Snecma
- SRI International
- The University of Akron – Dr. Wieslaw K. Binienda
- Williams International

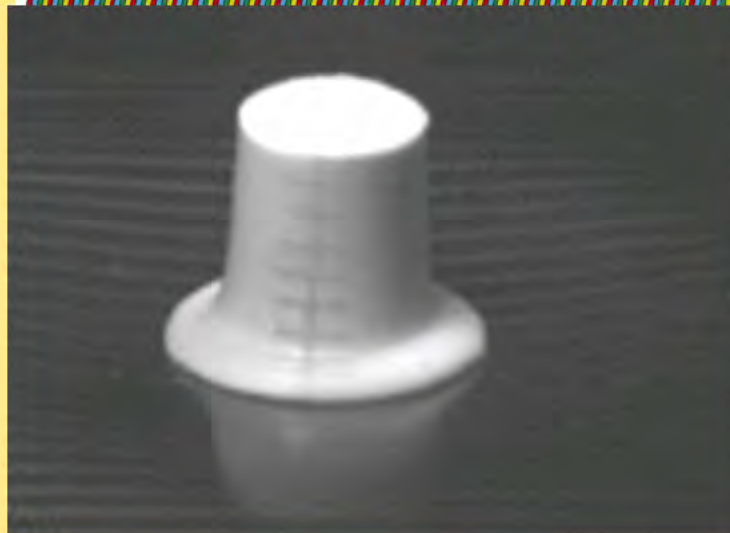
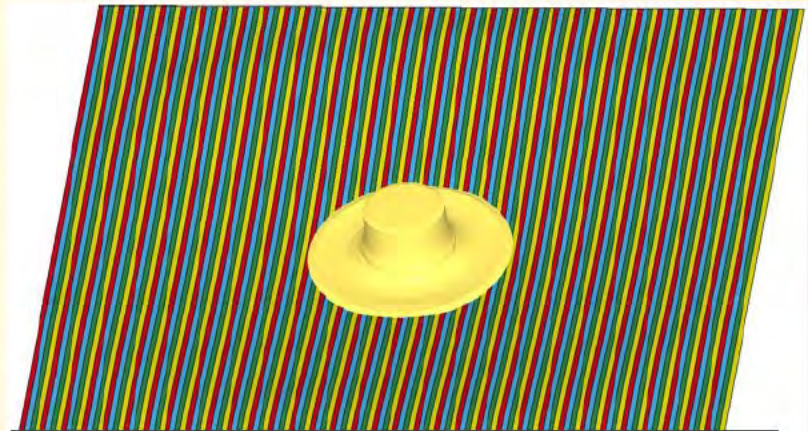
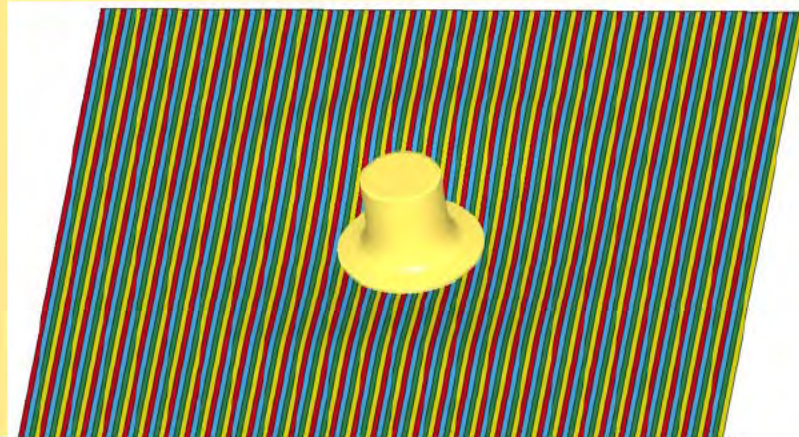
Impact Video of (0+/-60) Composite Panel (Velocity below penetration threshold)



$V = 491 \text{ ft/s (150 m/s)}$

(Test LG380, 7,100 pps)

Methodology



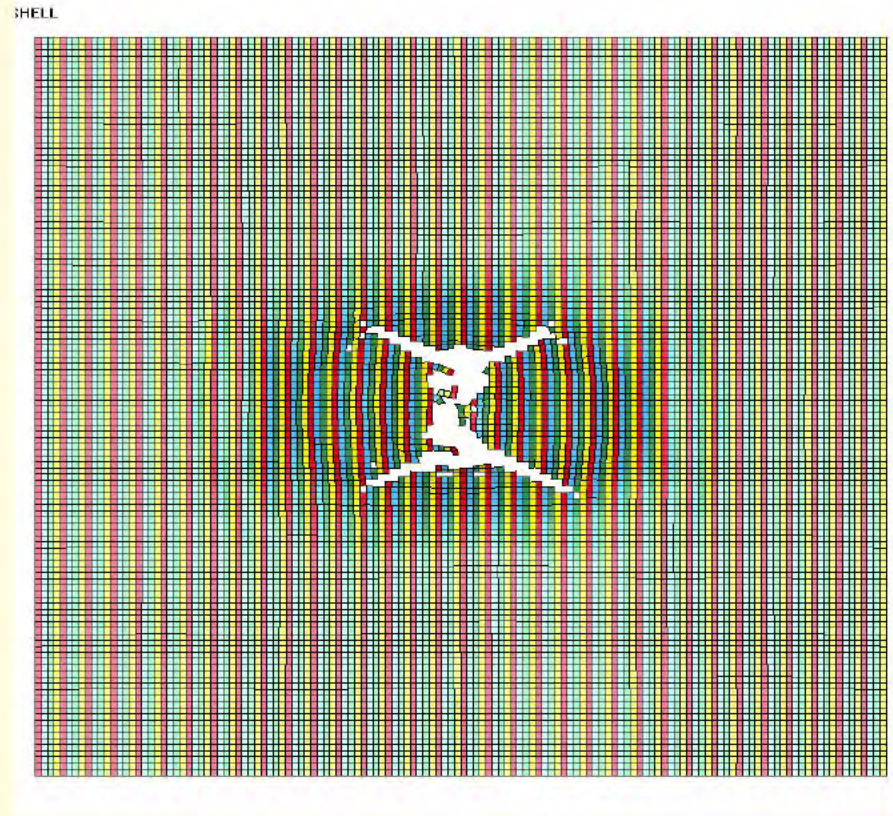
Methodology



Front



Back



0° / ±60° Composite plate after impact at 630 ft/s

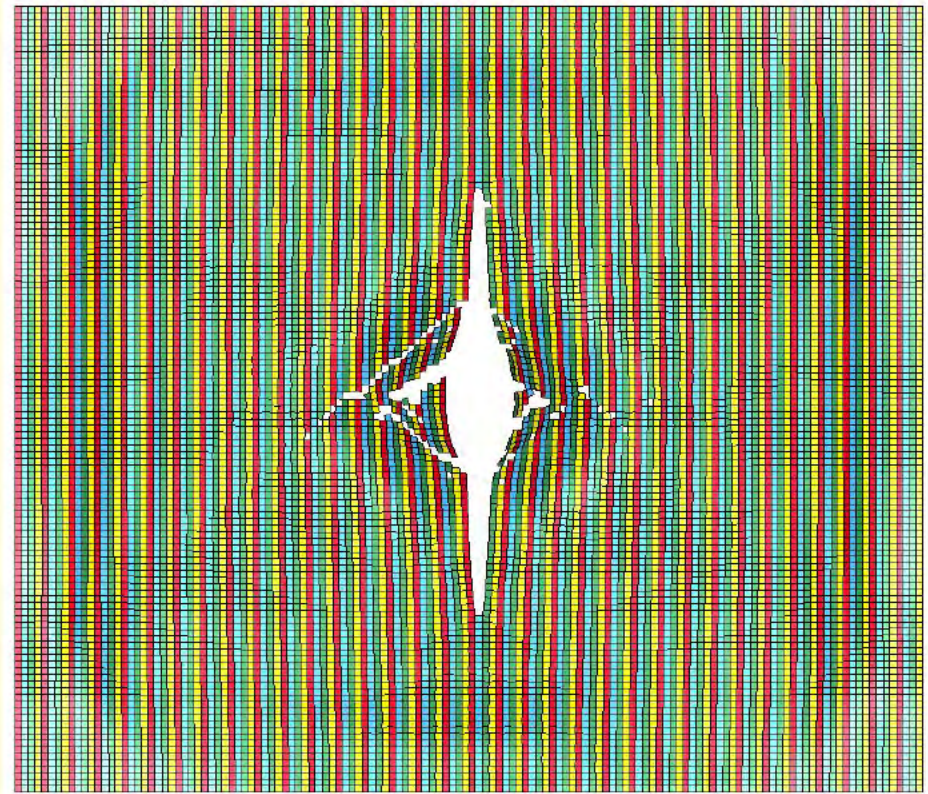
Methodology



Impact Velocity = 740ft/s



Impact Velocity = 823t/s

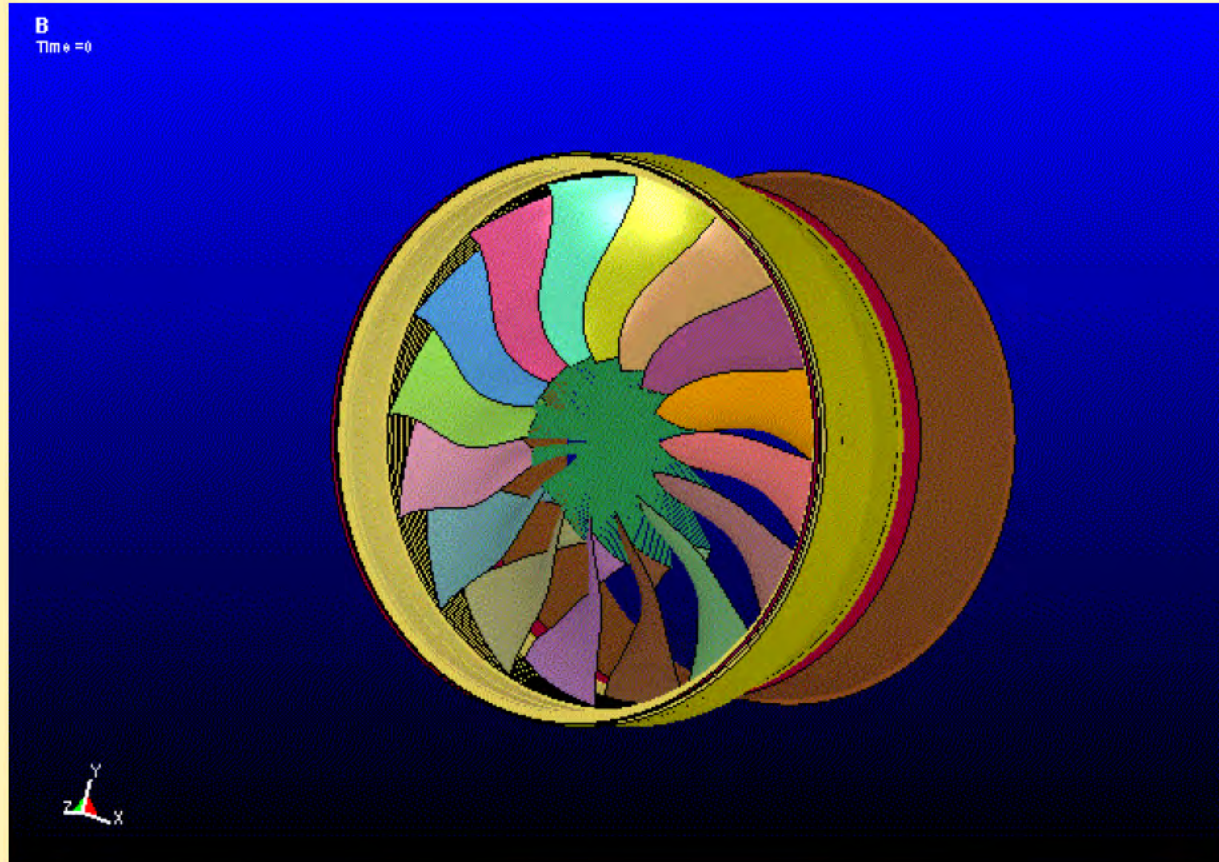


0°/±45° Composite plate after impact

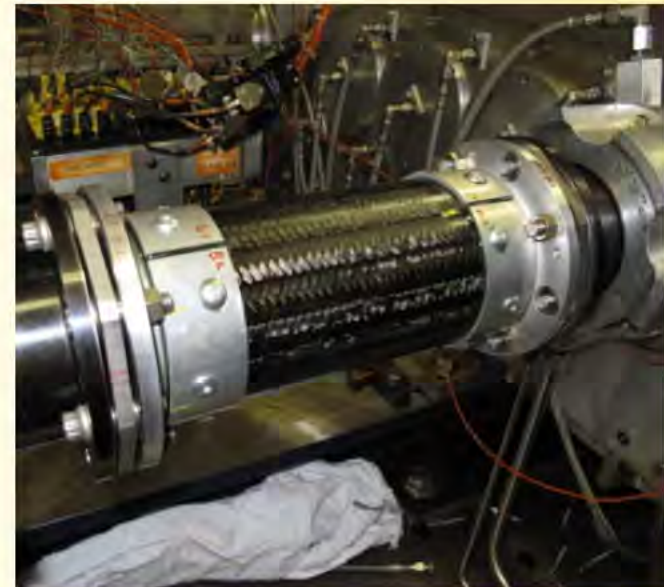
FAA Blade-out Test



STRUCTURE - Blade-out Test Simulation



Aerospace Applications



- Composite fan blade and containment structures such as GEnx engine (top left)
- Composite drive system such as shafts (top right), gears, and cases
- Composite airframe structures such as the fuselage frames on Boeing 787

Background Information on Smolensk Crash

Russian Investigating Committee Final Report on the Crash of Polish Tu-154M on April 10, 2010 in Smoleńsk

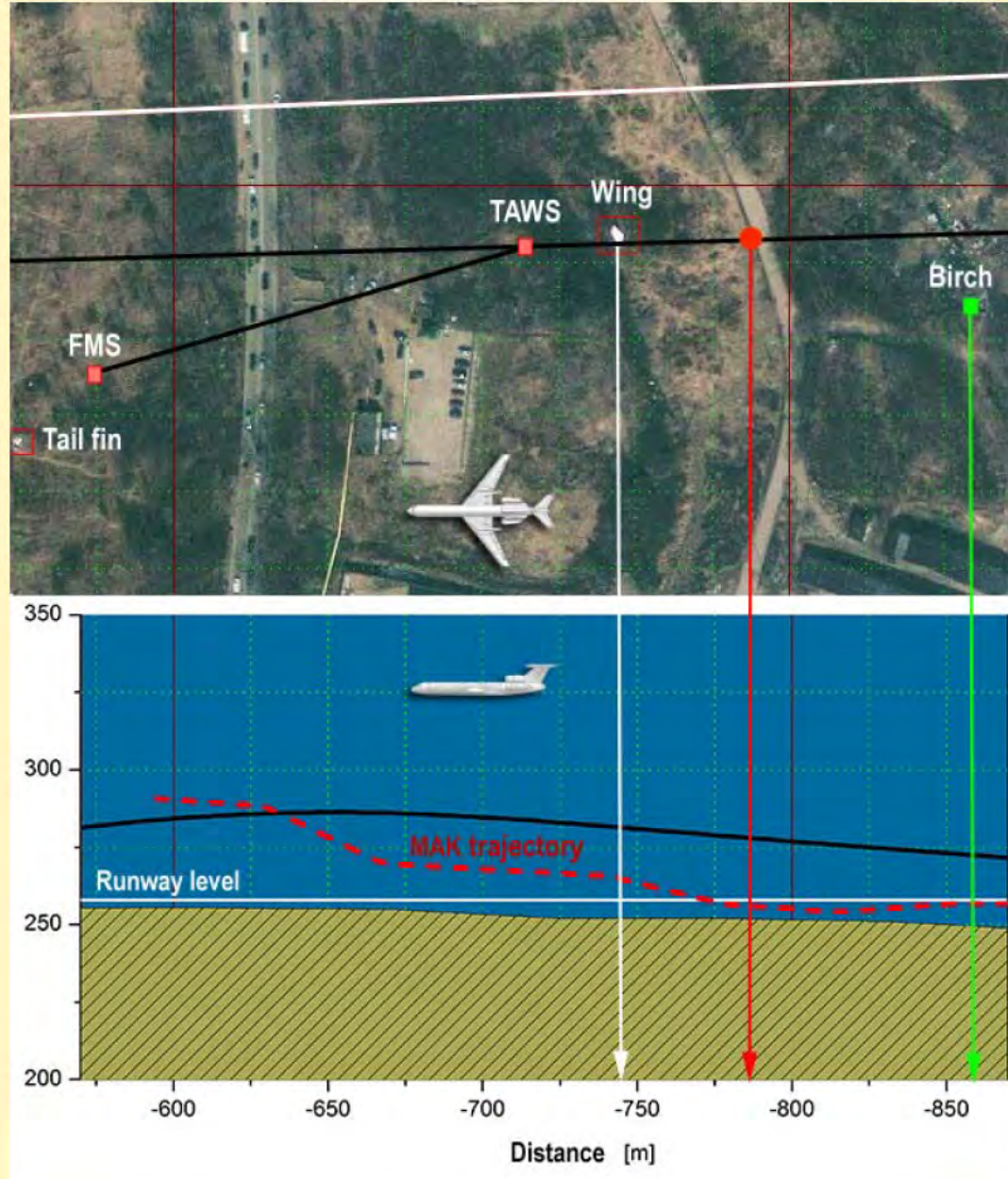
Section 3.1.69

- The aircraft collided with the birch with a trunk diameter 30-40 cm, which led to the left outer wing portion of about ~~4.7~~ 6.5 m long ripped off and intensive left bank.

Section 3.1.70

- In 5-6 more seconds, inverted the aircraft collided with the ground and was destroyed

Last Seconds Before the Crash





Satellite Images of the Area Where the Last TAWS Event Has Occurred (April and June 2010)

April 2010



June 2010



Material Parameters – Dry Birch Wood

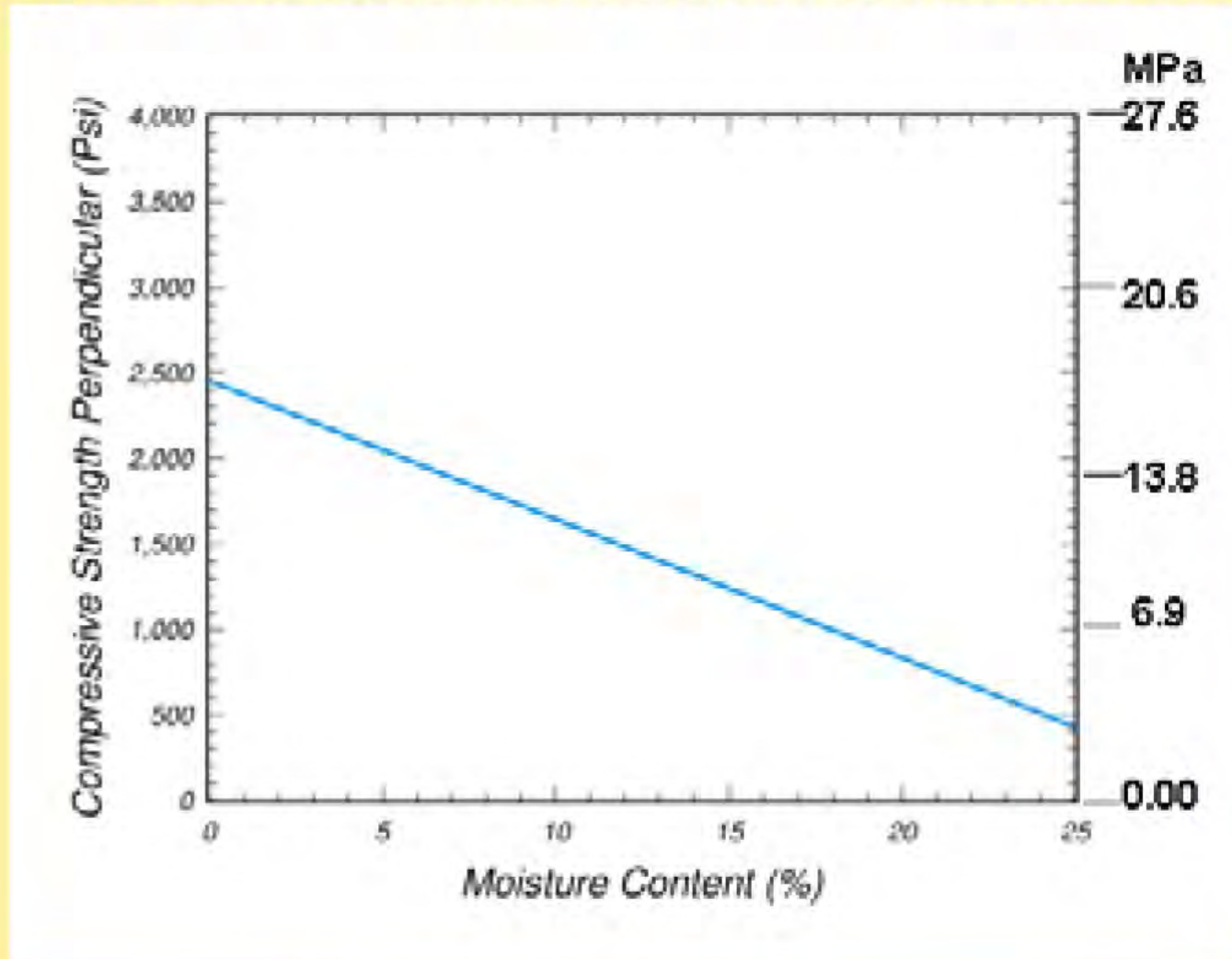
	Young's Modulus (MPa)			Poisson Ratio			Shear Modulus (MPa)			Density
	E_L	E_R	E_T	ν_{LT}	ν_{RL}	ν_{RT}	G_{TL}	G_{LR}	G_{RT}	(Kg/m ³)
Generic 4x	16000	1600	1100	0.451	0.043	0.697	700.4	762.2	175.1	1000

- **Generic Birch Model: elastic, cylindrically, orthotropic (Failure Max Strain)**
- **Mat143 - New Birch Model: nonlinear (Modified Hashin)**

MAT143										
mid	ro	nplot	iters	irate	hard	ifail	ivol			
6	700	1	1	1	0	0	0			
el	et	glt	glr	pr						
1.14E+10	2.43E+08	5.88E+08	8.70E+07	0.39						
xt	xc	yt	yc	sxy	syz					
1.61E+08	3.59E+07	3.45E+06	3.75E+06	9.90E+06	1.40E+07					
gf1	gf2	bfit	dmax	gf1p	gf2p	dfit	dmaxp			
223.39999	838.4	3	0.99	2.1	7.88	3	0.99			
flpar	flparc	powpar	flper	flperc	powper					
4.50E-06	4.50E-06	0.107	9.62E-05	9.62E-05	0.104					
npar	cpar	nper	cper							
0.5	400	0.4	100							



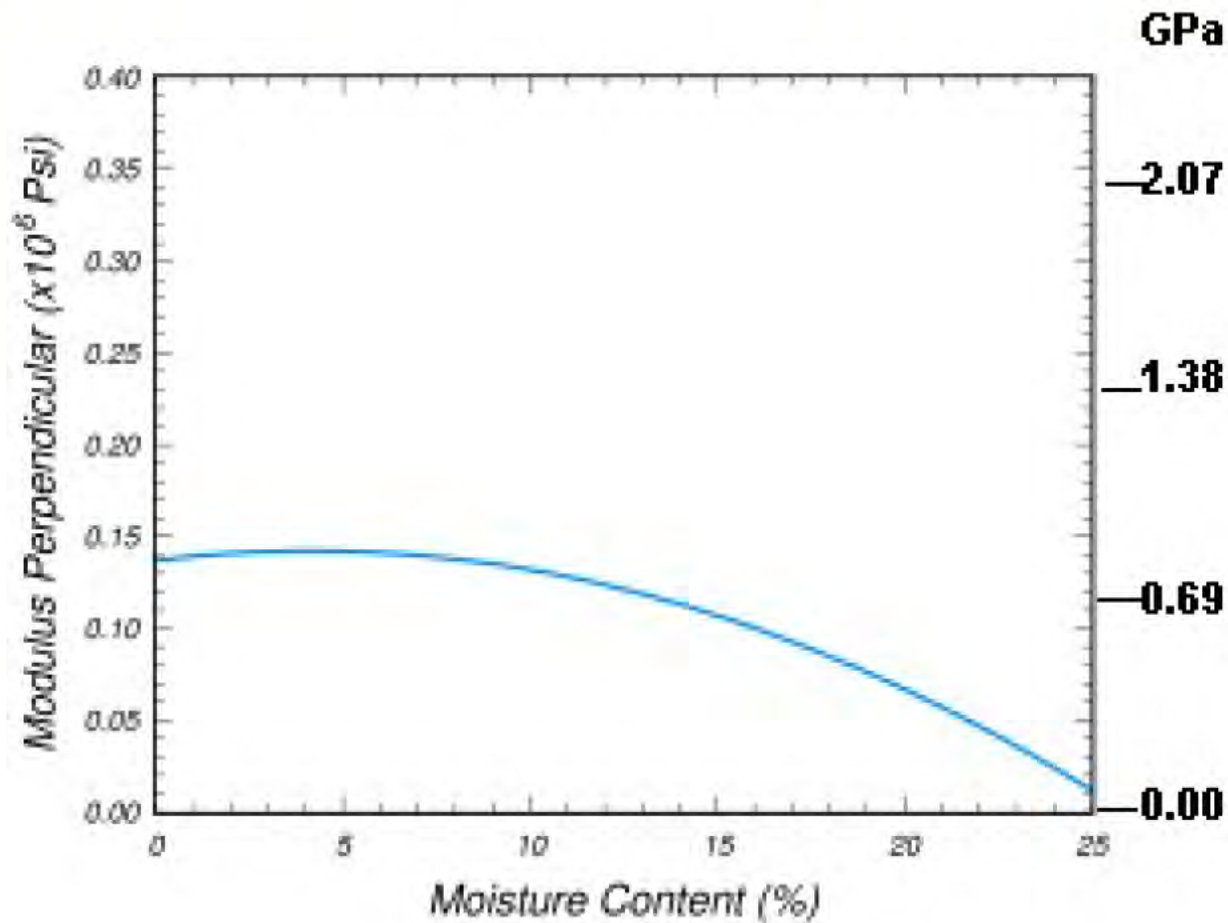
Wood Moisture Effect: The more humid wood the weaker it is!



Source: Forest Products Laboratory

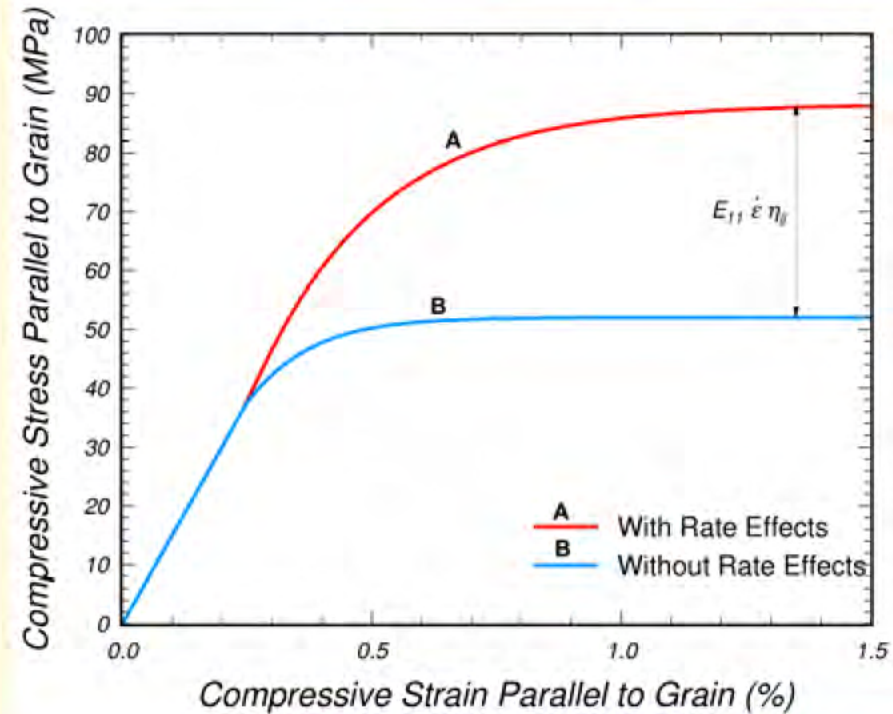
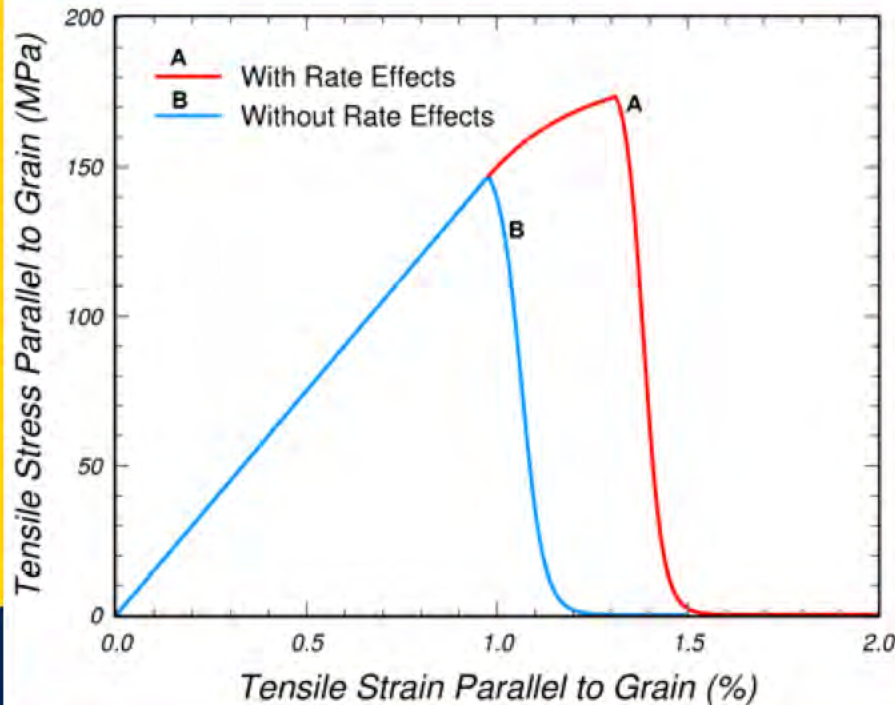
Wood Moisture Effect

The more humid wood the softer it is.



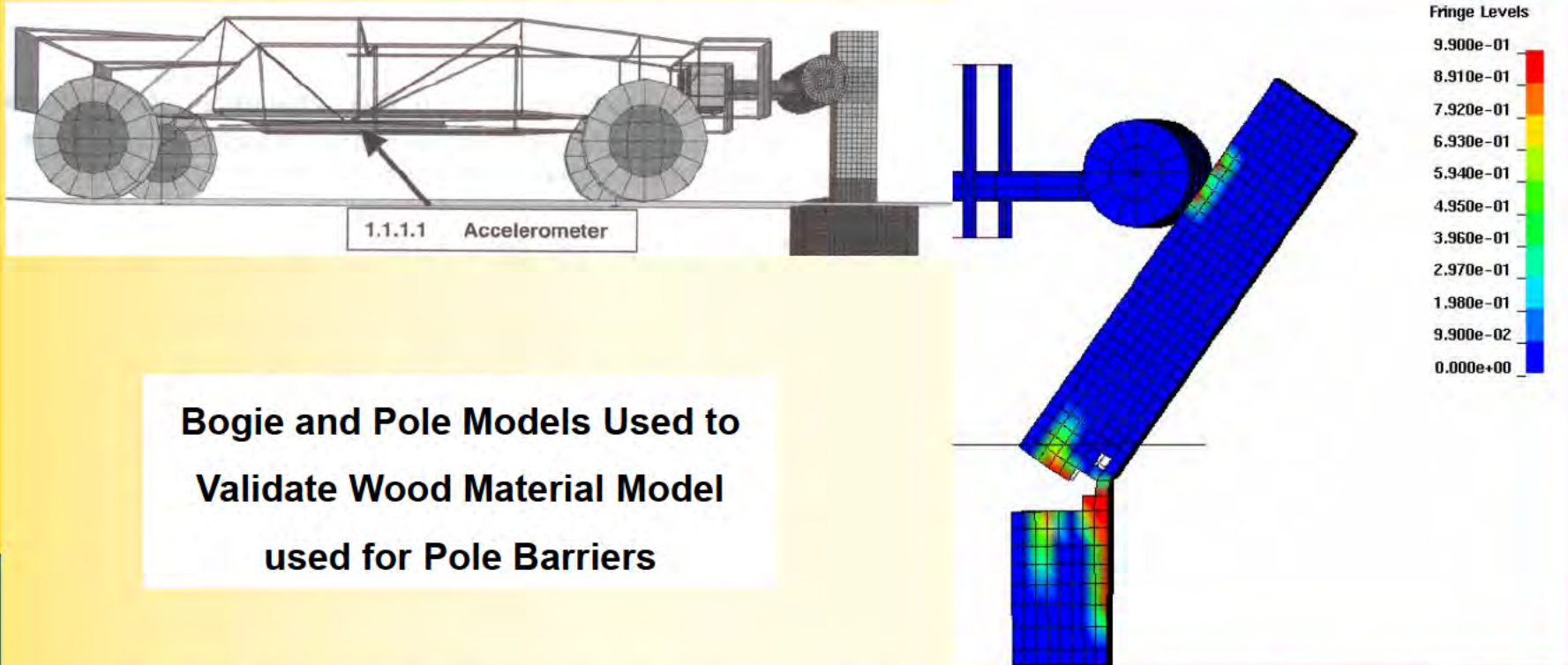
Source: Forest Products Laboratory

Wood Load Rate Effect



Based on Model developed by Federal Highway Administration (FHWA) **Manual for LS-DYNA Wood Material Model 143, Publication No. FHWA-HRT-0R-097, Aug. 2007**

Validation of the State of the Art Nonlinear Wood Model (Mat143) using FHWA Vehicle Crash Test

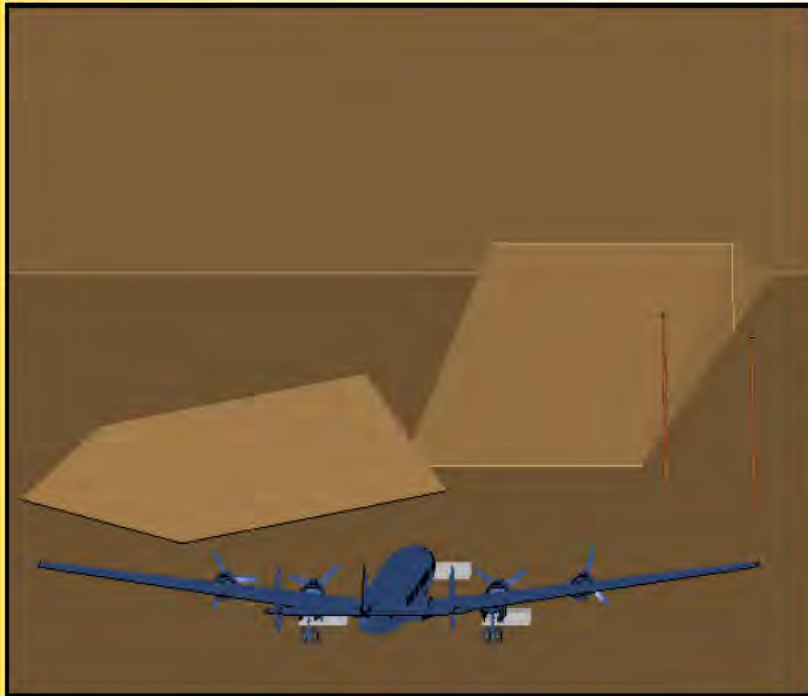


Bogie and Pole Models Used to Validate Wood Material Model used for Pole Barriers

Note: Pole model breaks without any splinters due to the homogenized (Macro-level) material model

Manual for LS-DYNA Wood Material Model 143, Publication No. FHWA-HRT-0R-097, Aug. 2007

Validation of the Mat143 using FAA Test - 1965



Simulations Authors: Robert T. Bocchieri, Robert MacNeill, Claudia Navarro-Northrup, Douglas S. Dierdorf.

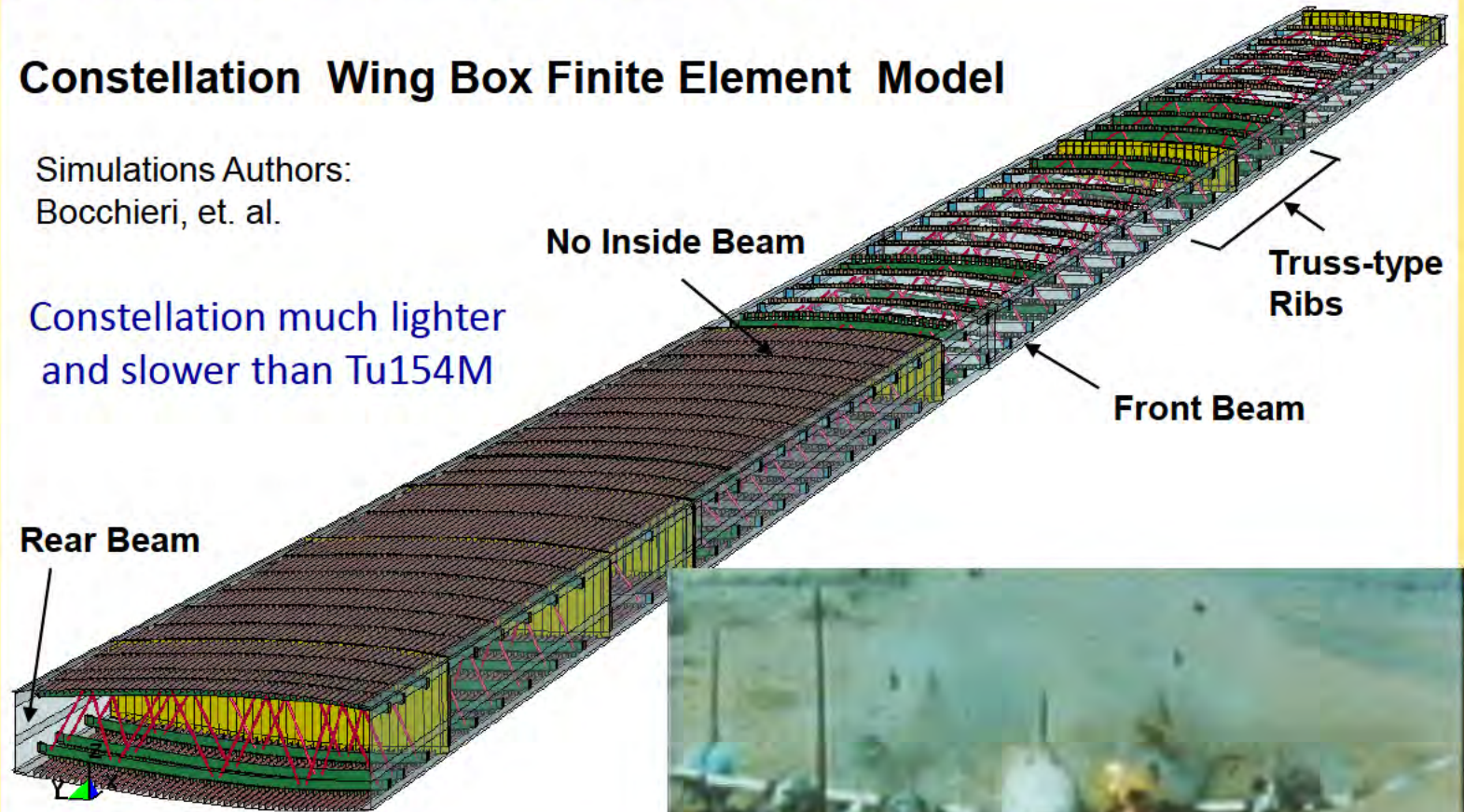
- Mass of the airplane 40T, initial impacts at 112 knots (207 km/h) sheared the landing gear causing the aircraft to be airborne and slide on its belly.
- The left wing struck an earthen barrier and the right wing struck two vertical telephone poles.

Application of the Wood Model to Lockheed Constellation Model 1649 Test

Constellation Wing Box Finite Element Model

Simulations Authors:
Bocchieri, et. al.

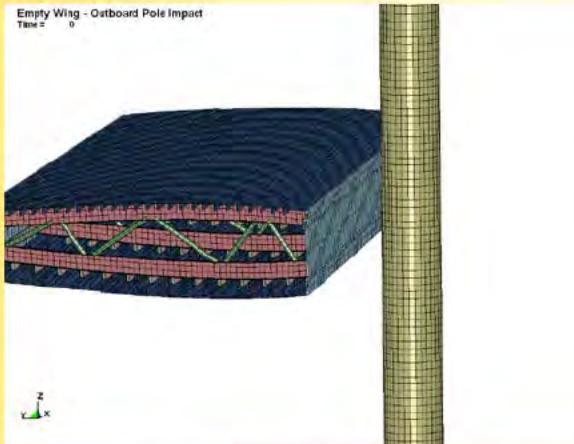
Constellation much lighter
and slower than Tu154M



Reed, W.H., S.H. Robertson, L.W.T. Weinberg, L.H. Tyndall, "Full-scale Dynamic Crash Test of a Lockheed Constellation Model 1649 Aircraft", FAA-ADS-38, October, 1965.

Validation of Nonlinear Wood Model

Simulations by the Applied Research Associates



Simulations' Authors: Bocchieri, et. al.

Outboard Pole Impact

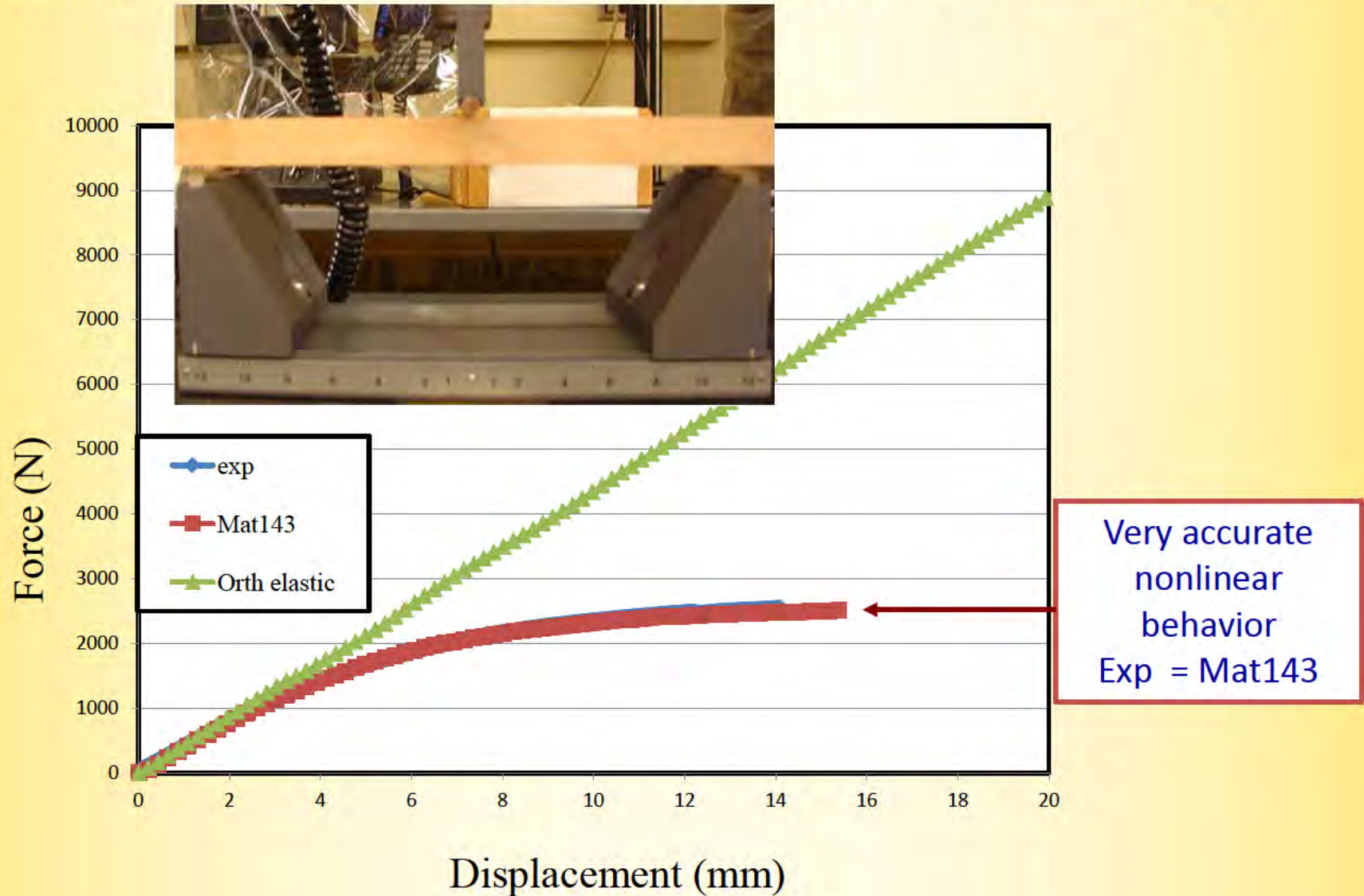
Inboard Pole Impact



Simulation Agreed with FAA Experiment

- Inboard pole is cut by the wing
- Inboard tank compromised after impact with ground
- Outboard tank damaged by impact with the second pole, outboard pole is also cut
- Both poles fell in the direction of the airplane movement

Validation of the Original and Nonlinear Wood Models using Birch Three Point Bending Test



Parameters of the Aluminum Tu-154

- Parameters of Aluminum D16, V95, AK6, etc.
<http://www.splav.kharkov.com/en/>

Generic AL Material Density(Kg/m ³)	Young's modulus, E(Pa)	Yield Stress(Pa)	Tangent Modulus, Ec (Pa)	Poisson Ratio, v	Failure Strain
2850	7.4E+10	4.44E+8	5.738E+8	0.33	0.14

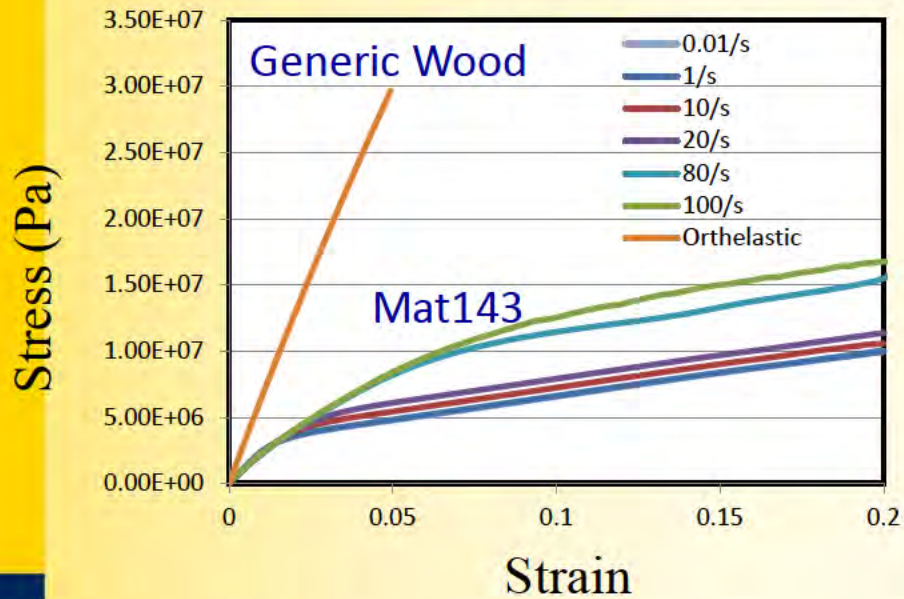
■ Aluminum:

- **Original** - isotropic, elasto-plastic hardened (Max Strain)
- **Johnson-Cook** - nonlinear, strain rate dependent

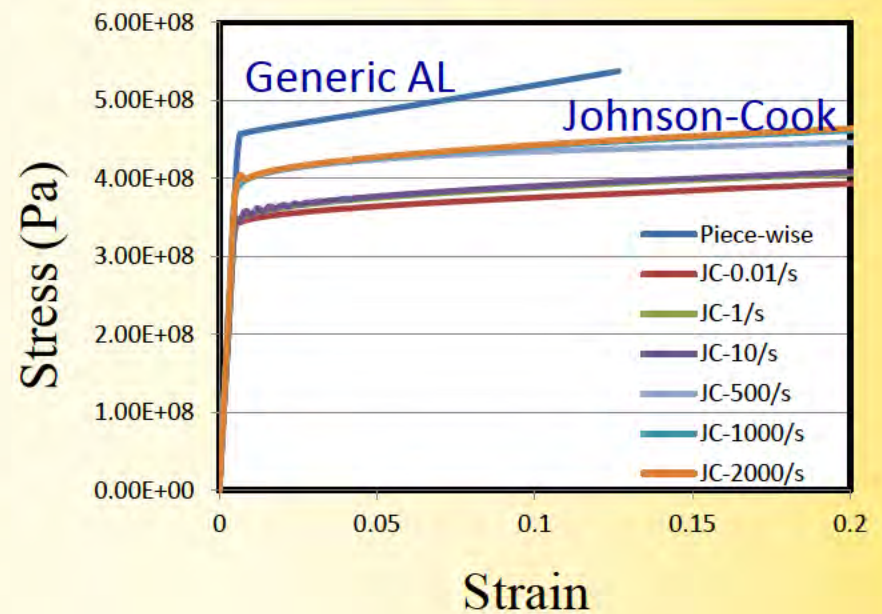
*MAT_JOHNSON_COOK							
mid	ro	g	e	pr	dtf	vp	rateop
4	2700	2.59E+10	6.89E+10	0.33	0	0	0.1
a	b	n	c	m	tm	tr	epso
3.24E+08	1.14E+08	0.42	0.002	1.34	925.16	193.16	1.00E-05
cp	pc	spall	it	d1	d2	d3	d4
0	0	2	0	0.13	0.13	-1.5	0.011
d5	c2/p	erod	efmin				
0	0	0	0				

Plots for the Birch Wood and Aluminum Strain Rate Effect

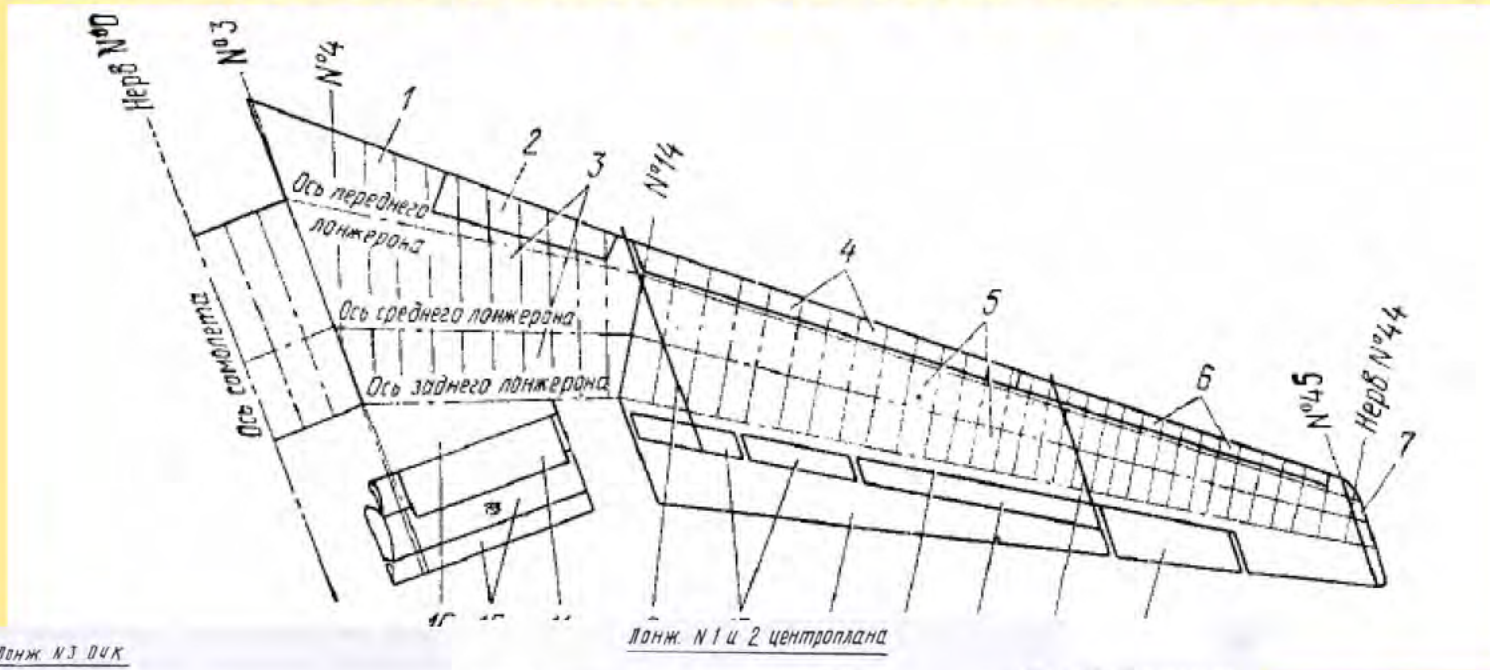
Birch Wood



Aluminum

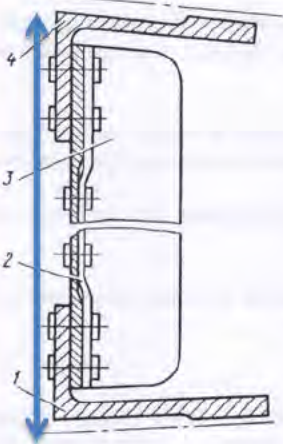


Internal Structure of the Tu-154M Wing



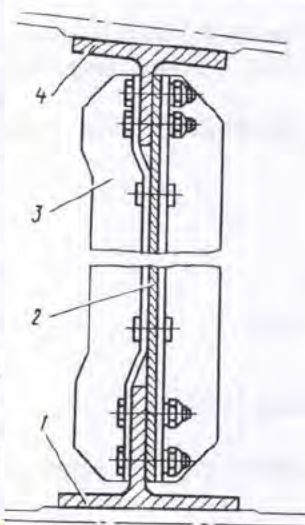
230mm

Лонж. №3 ОК

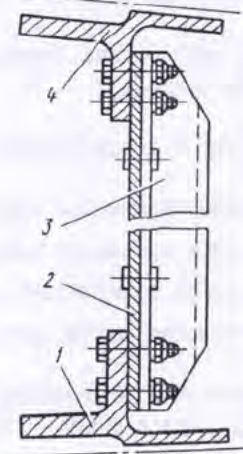


- 1. Нижний пояс
- 2. Стенка
- 3. Стойка
- 4. Верхний пояс

Лонж. №1 и 2 центроплана



Лонж. №3 центроплана

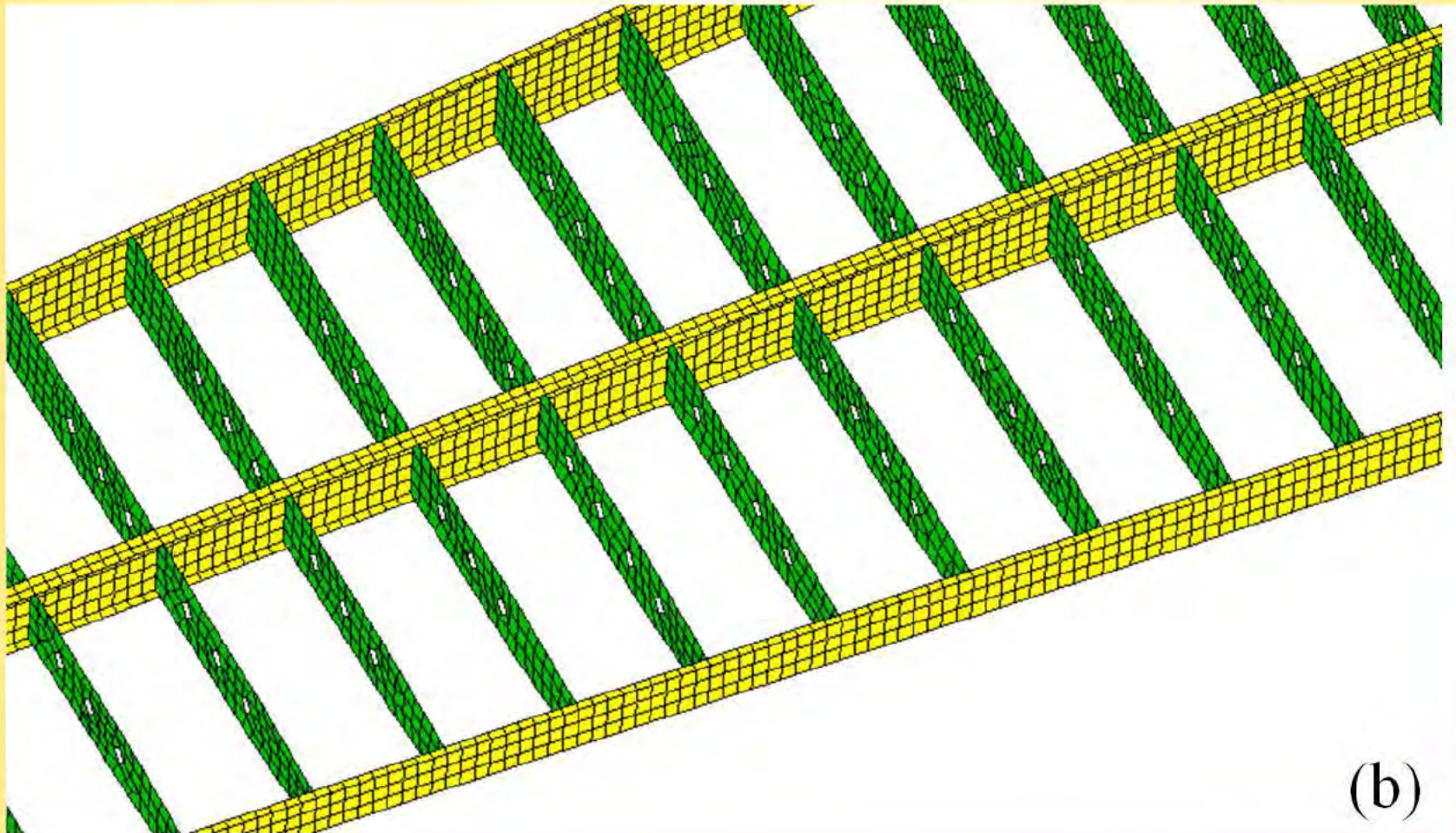


Boeing 727

Inner Structure of the Wing

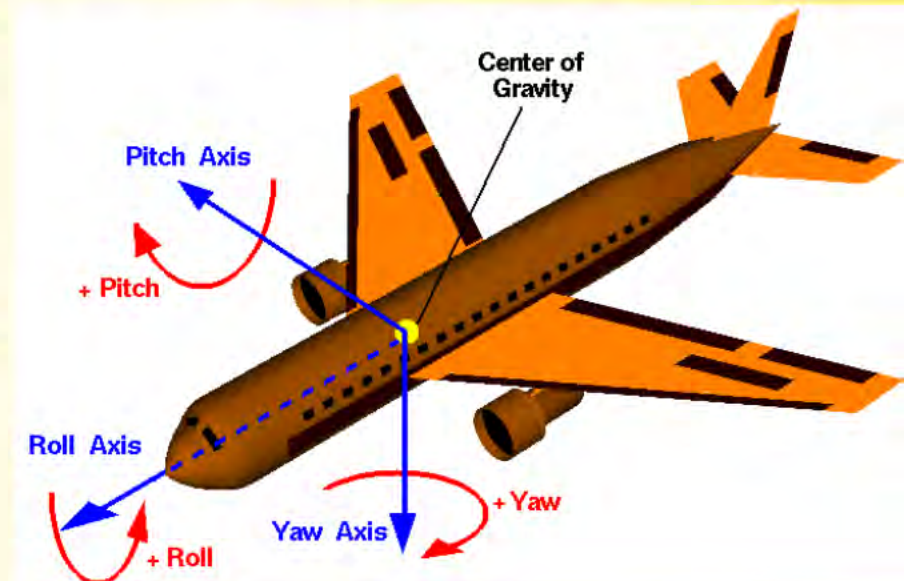


FEM Representation of Internal Structure of the Tu154M Wing



Input Parameters

- Velocity: **77-80 m/s horizontal, 0-19.2 m/s vertical up**
- Plane mass: **78600 kg**
- Distance from the base to the tree cut : **6.0m**
- Birch diameter at the cut section: **44cm**
- Birch density: **700 - 1000 kg/m³**
- Location of the impact on the wing from its tip: **6.5m**
- Several plane orientations:
 1. Horizontal
 2. Nose up: 5° – 20°
 3. Roll- 5° , horizontal
 4. Roll- 5° & pitch 5° – 20°

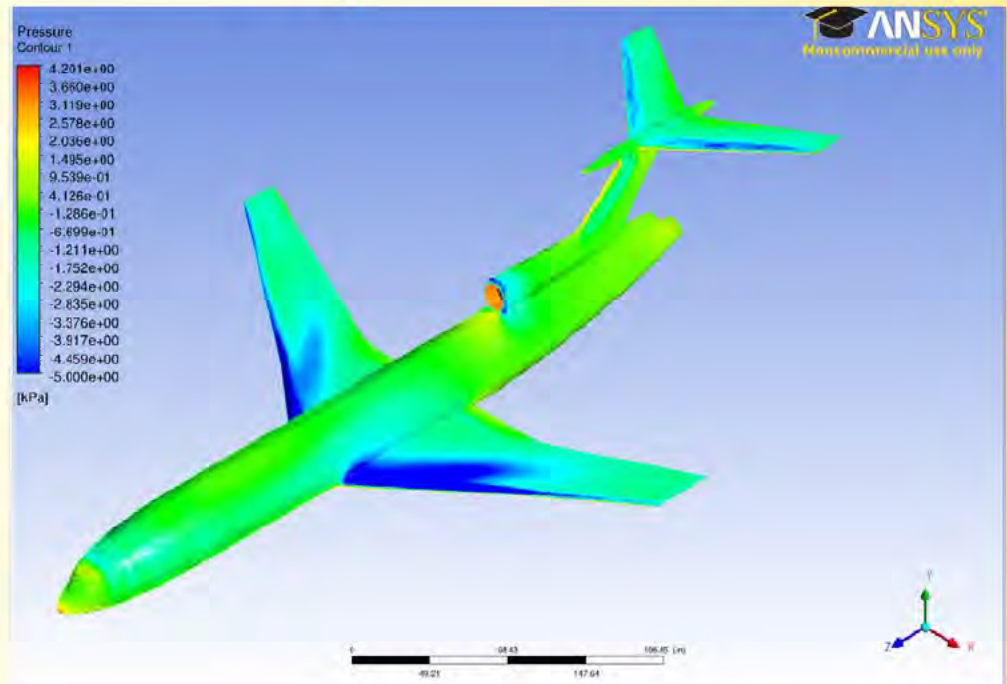


Math and Physics Background in CFX

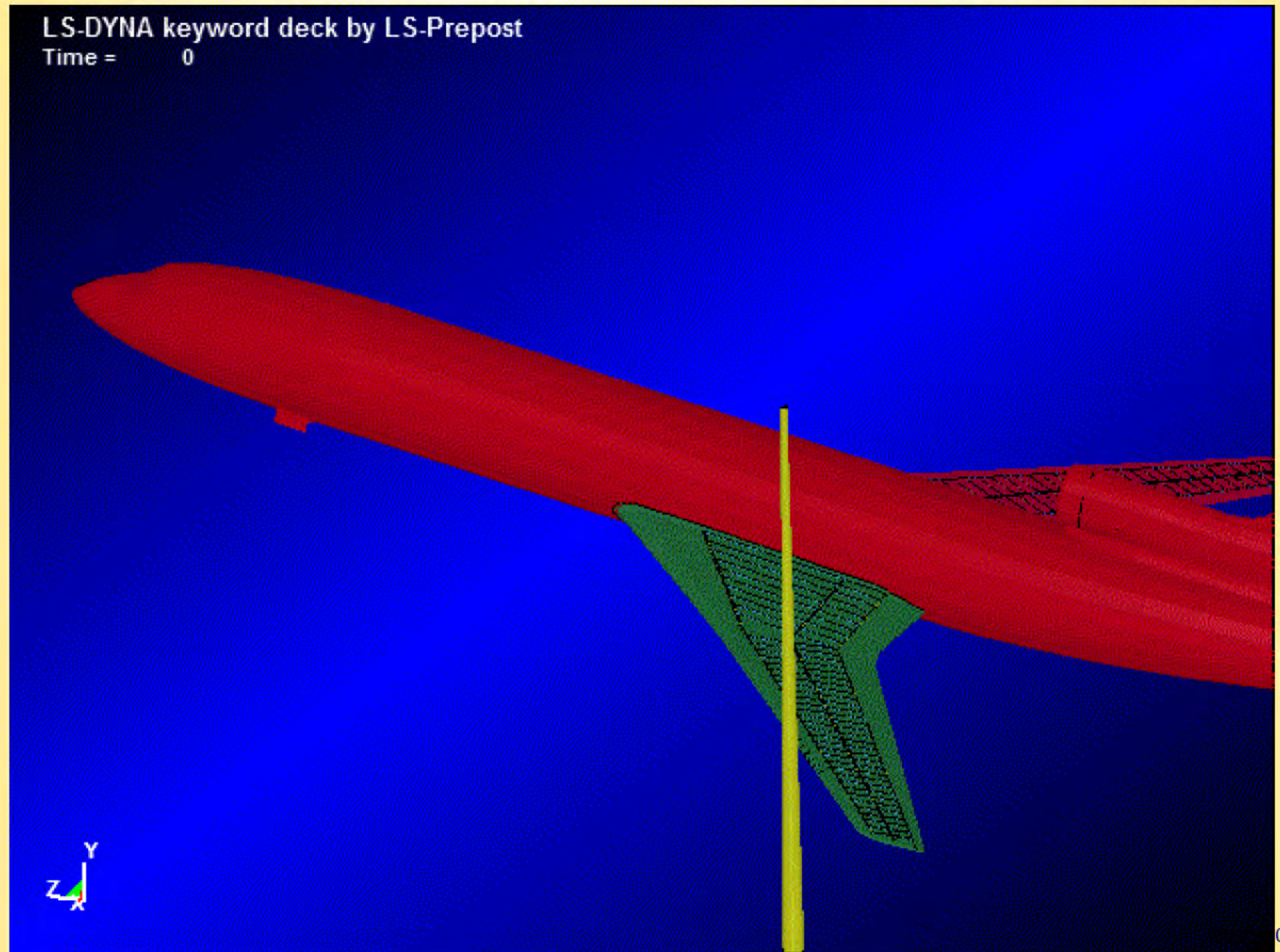
- Ansys- CFX analysis conducted by UA Research Fluid Mechanics Laboratory.
- Full form of Navier-Stokes equations with continuity of the flow.

$$\frac{\partial(\rho u_i)}{\partial t} + \nabla \cdot (\rho \vec{V} u_i) = -\frac{\partial p}{\partial x_i} + \nabla \cdot (\mu \nabla u_i) + S_{Mx_i}$$

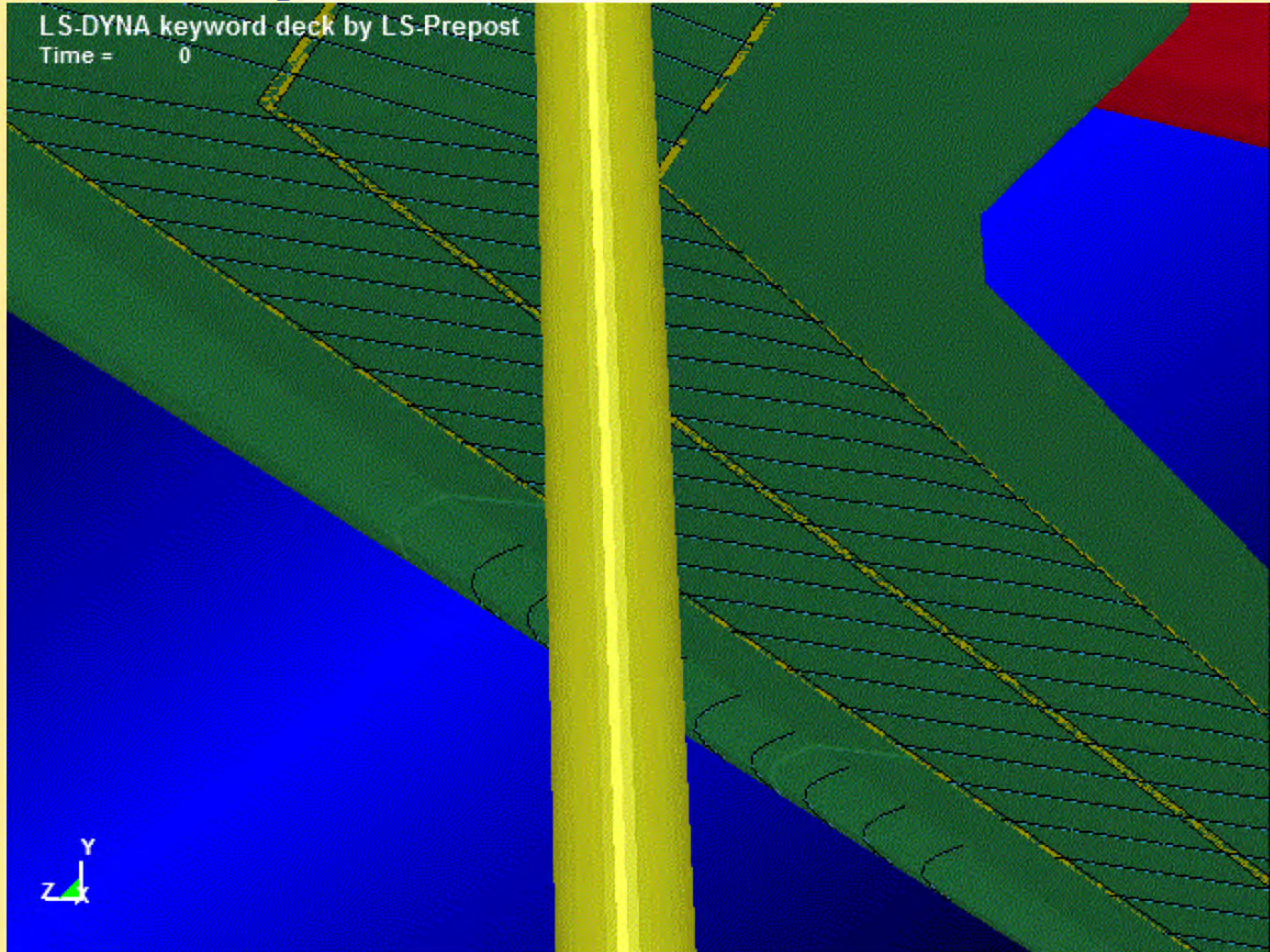
$$\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \vec{V}) = 0$$



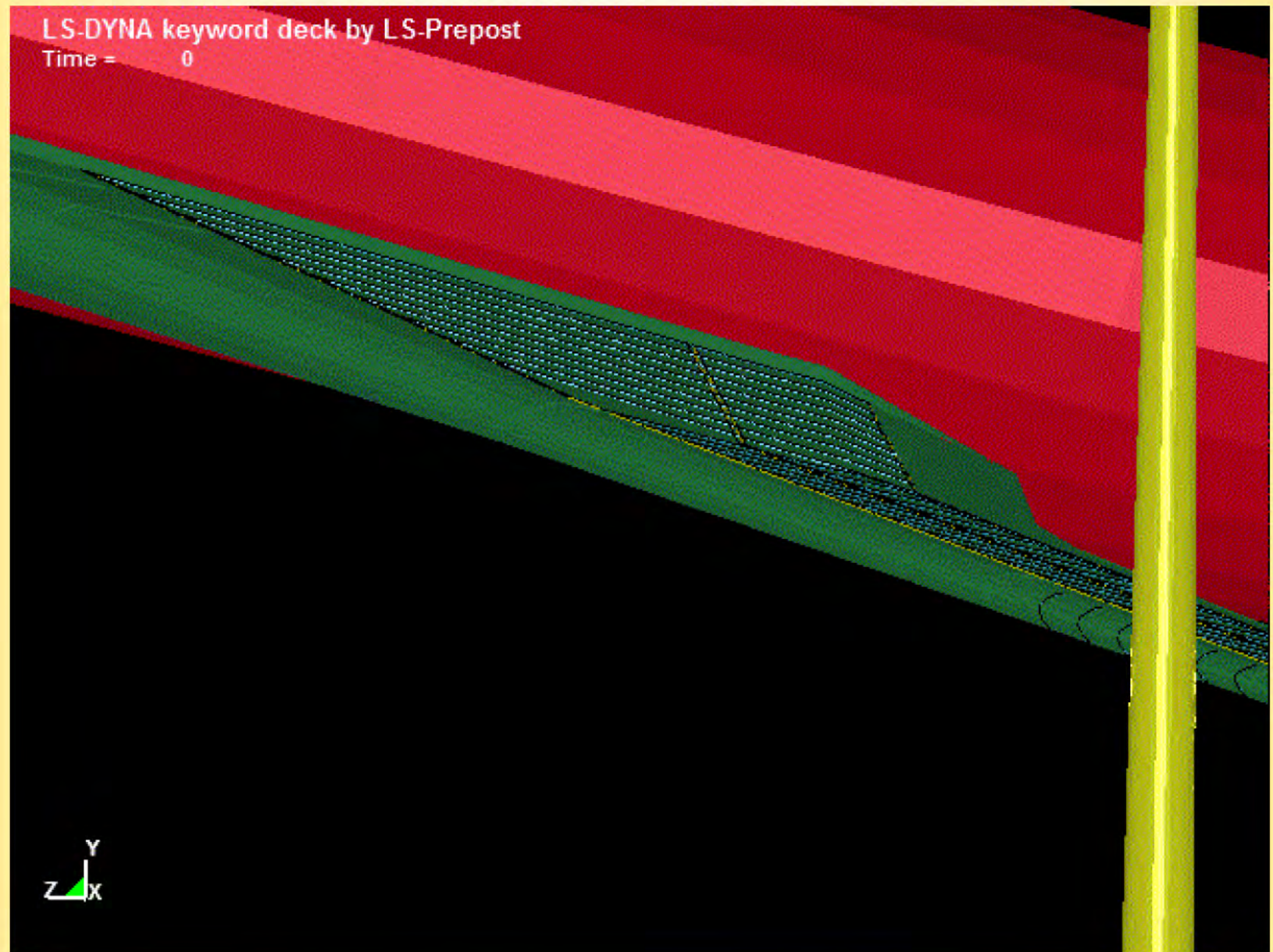
Simulation – view from the left side



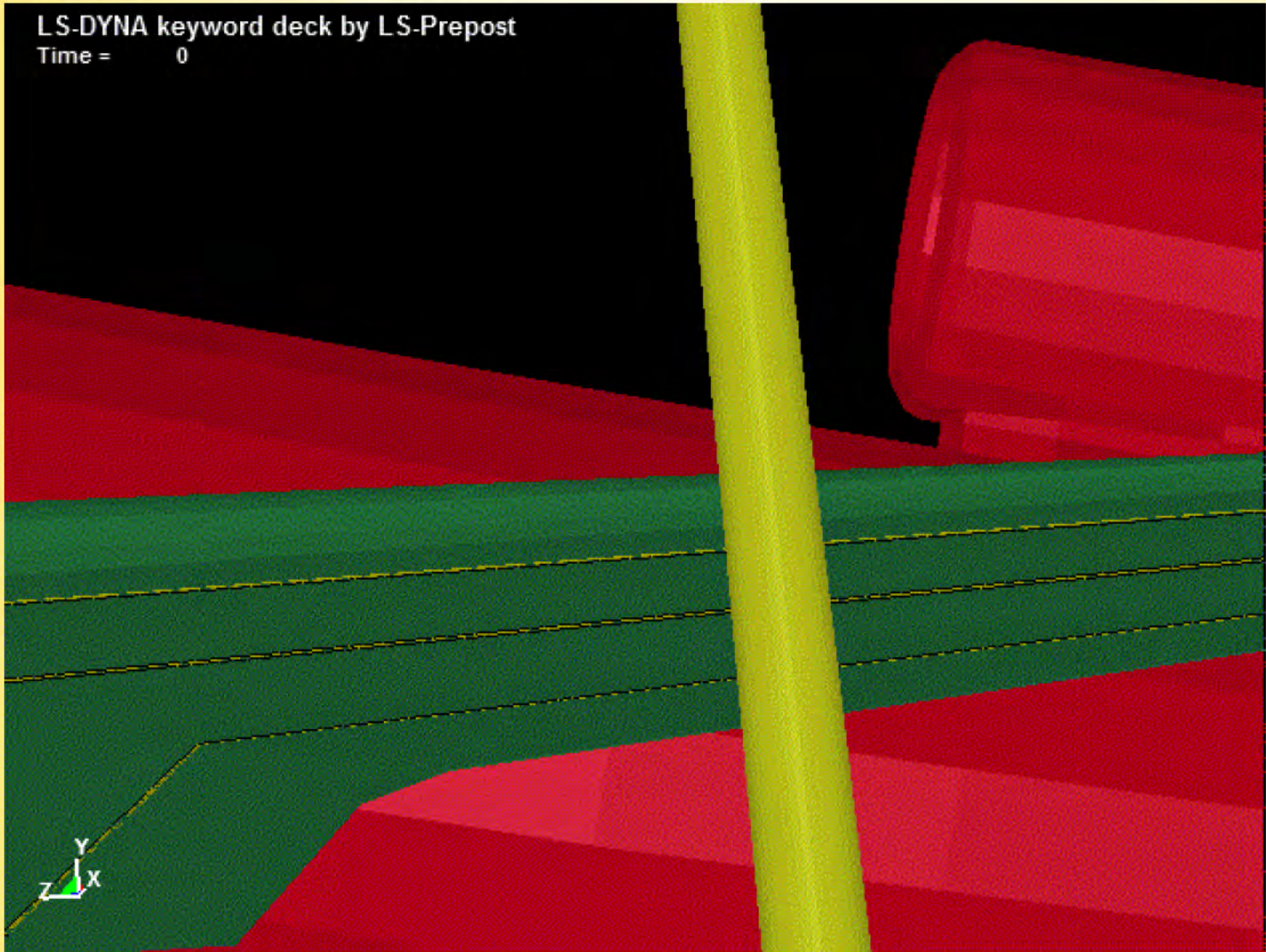
Close-up 1



Refined Case – Flight Horizontal, Mat143 and JC

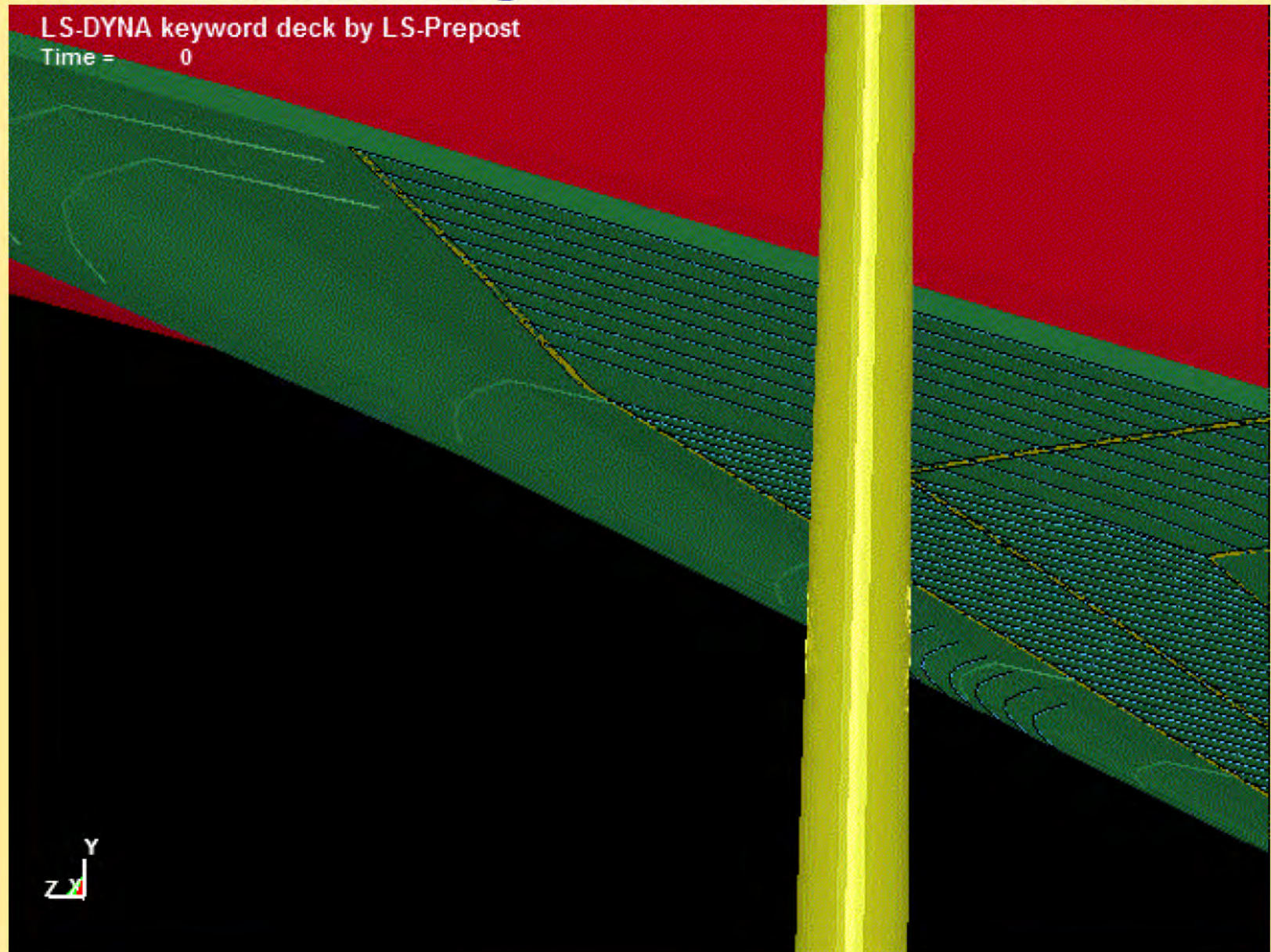


Refined Case – Flight Horizontal, Mat143 and JC



View from the bottom

Refined Case – Flight Inclined, Mat143 and JC



Conclusions from Wing/Birch Simulations

- Using parameters provided in the official Russian and Polish reports, the LsDyna Finite Element Method Model shows that:

THE WING OF THE TU-154M PLANE CUTS THROUGH THE BIRCH

- for every analyzed scenario
 - for all original & nonlinear rate dependent material models,
 - for the finest mesh.
- **THE DAMAGE TO THE WING IS LOCALIZED ON THE EDGE,**
DOES NOT DETERIORATE THE LIFT SURFACE OF THE WING, THUS
SHOULD NOT SIGNIFICANTLY REDUCE THE ABILITY OF THE PLANE TO FLY.

Above simulations have been positively evaluated by

BOEING Principal Structural Engineer

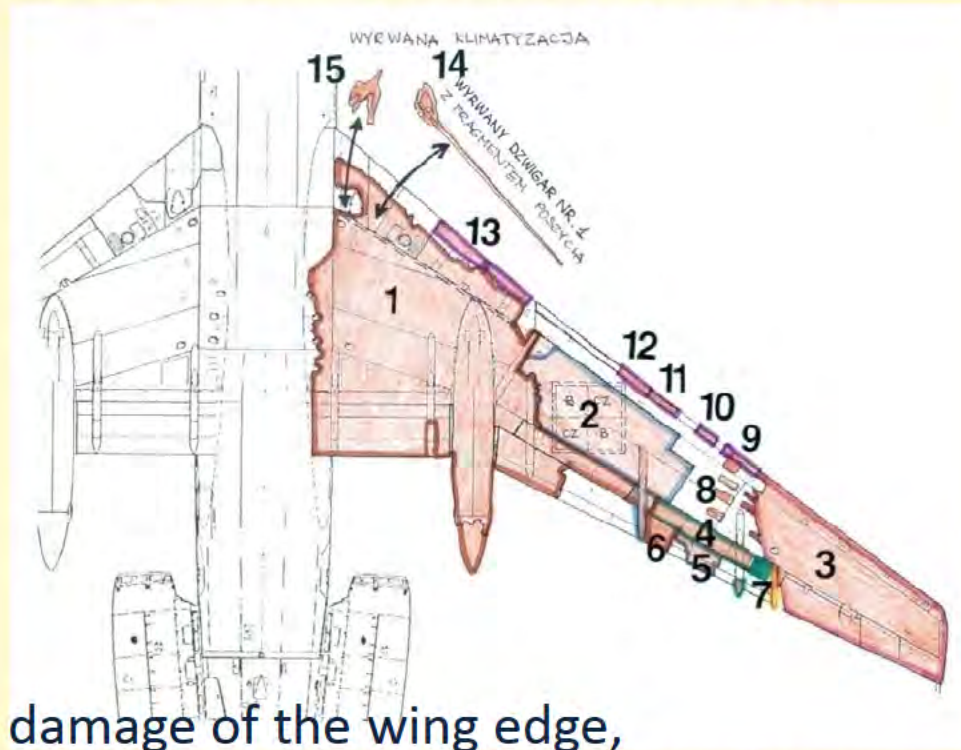
Dr. Wacław Berczynski.

Front Slots are not Destroyed!



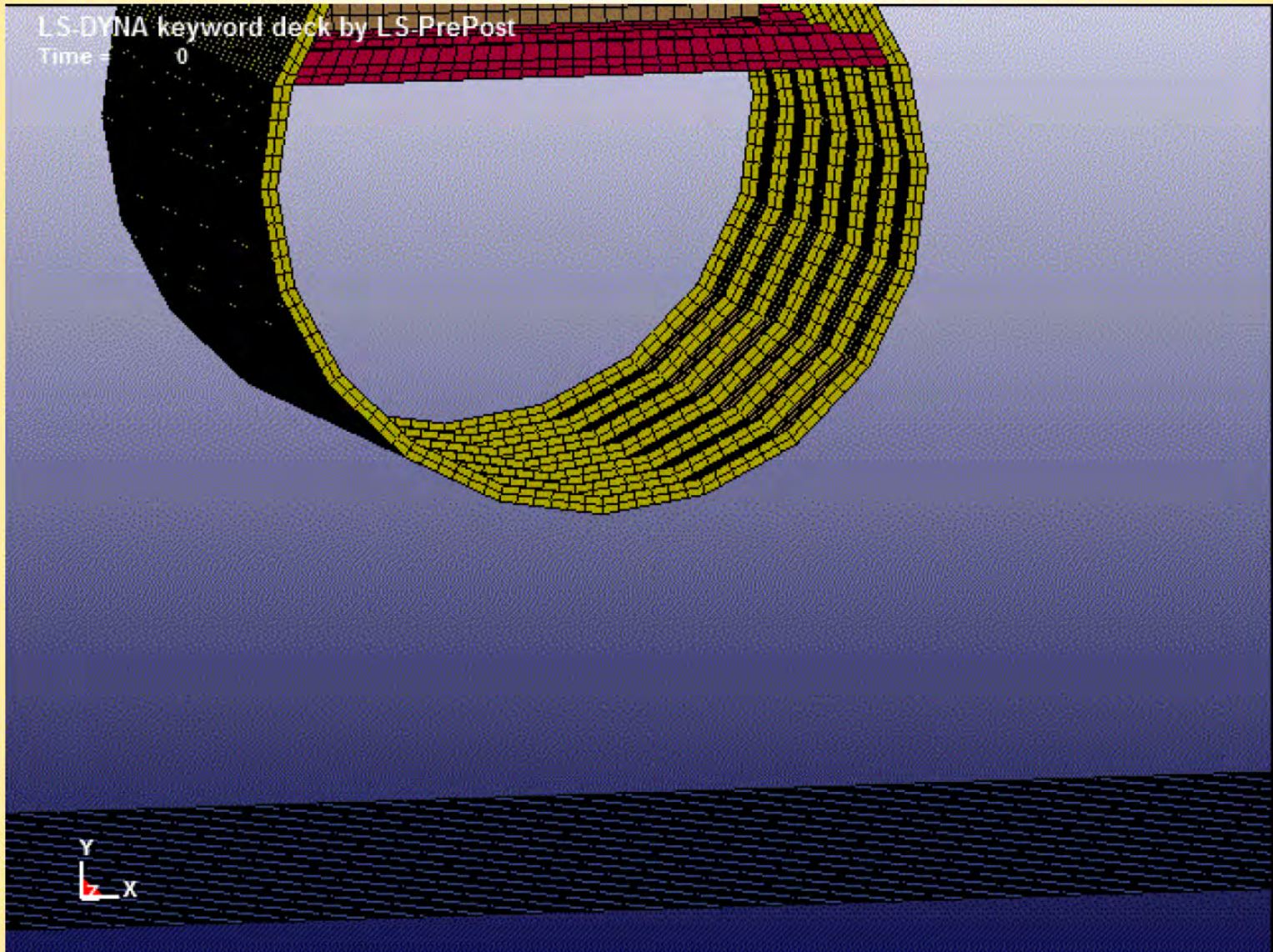
jumawa

Left Wing Reconstruction View From the Bottom Up



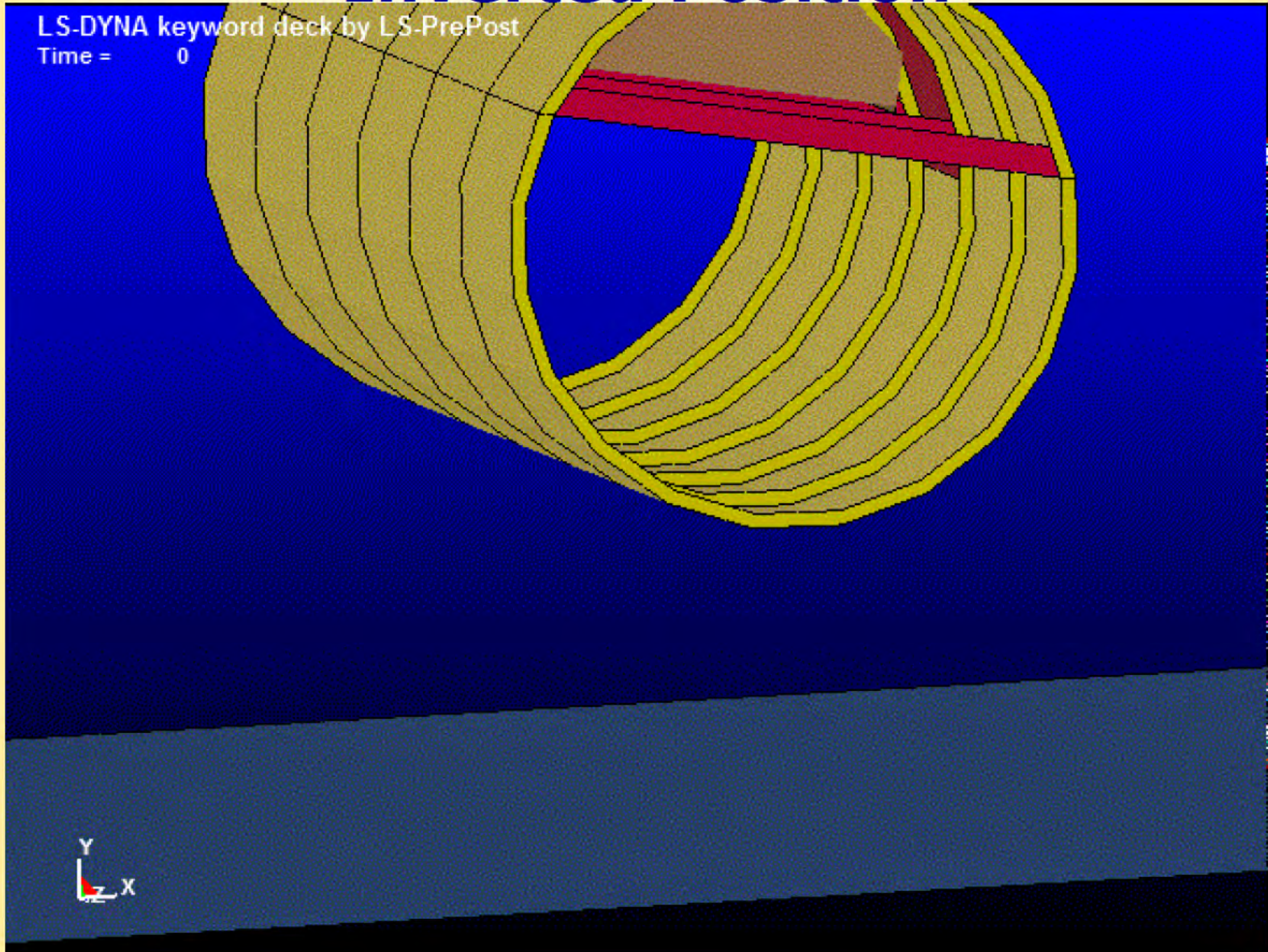
- There is no visible damage of the wing edge,
 - real tree lays perpendicular to the airplane flight direction, and
 - there is an extensive internal wing damage including ripped off rivets
- suggest:
- there was no impact between the birch tree and the left wing, and
 - an explosion near the point TAWS could explain the damage of the wing
 - and rapid turn left of the airplane

Vertical Drop of the Fuselage at Inverted Position

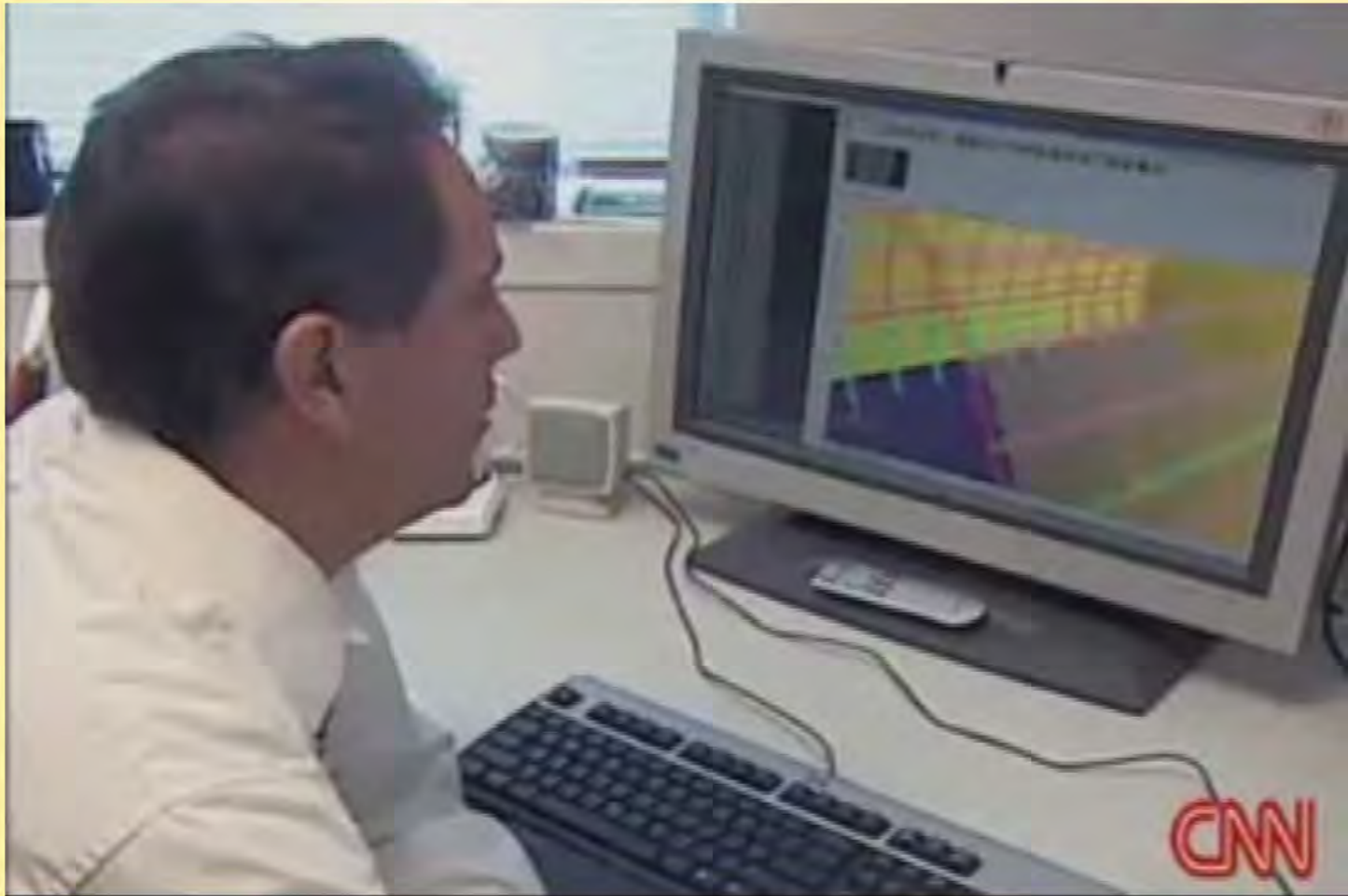


Vertical Impact with $v_y = -9.8\text{m/sec}$

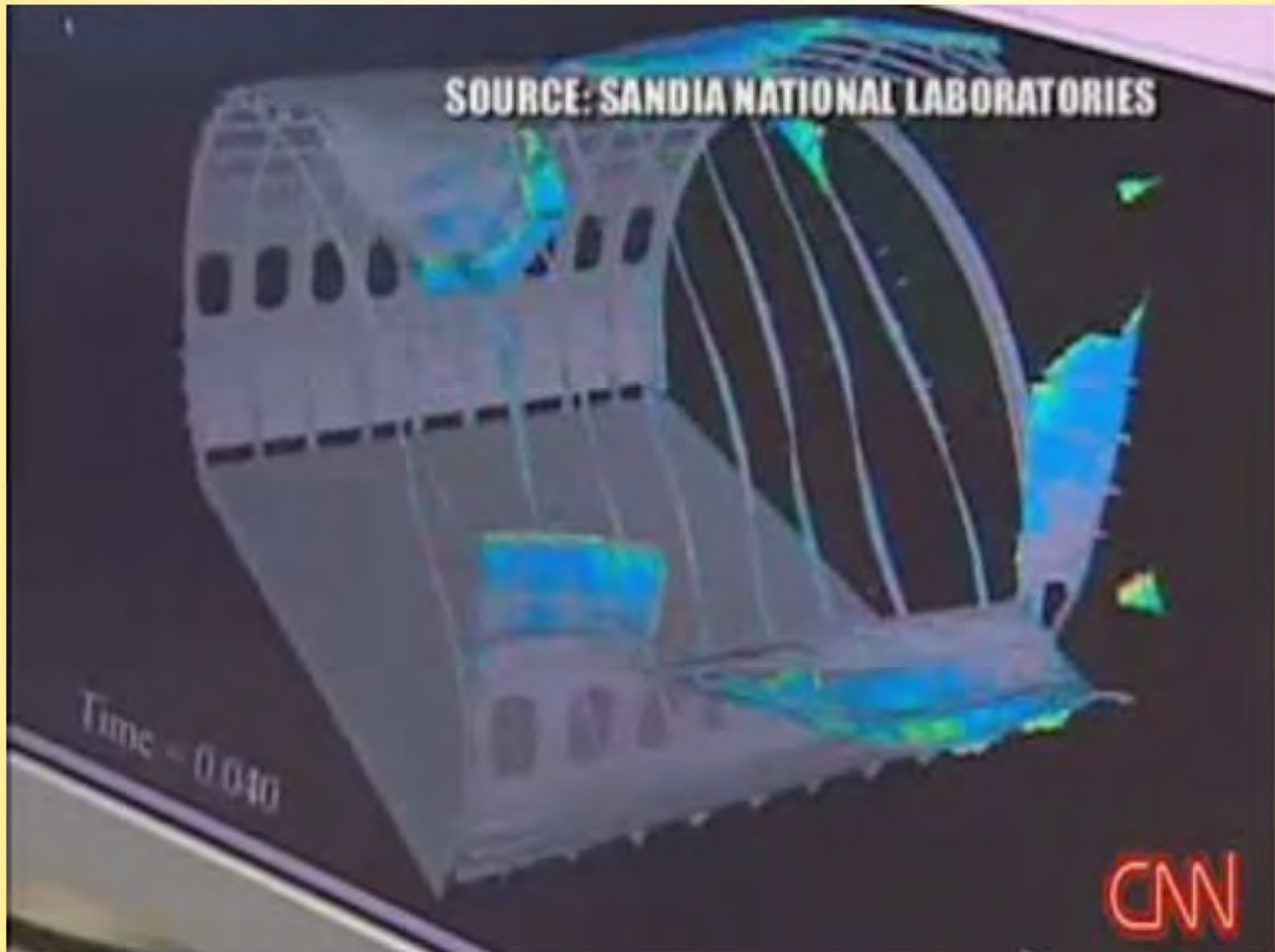
Vertical Drop of the Fuselage at Inverted Position



Simulation of Fuselage with Explosion Sandia National Lab – CNN 2008



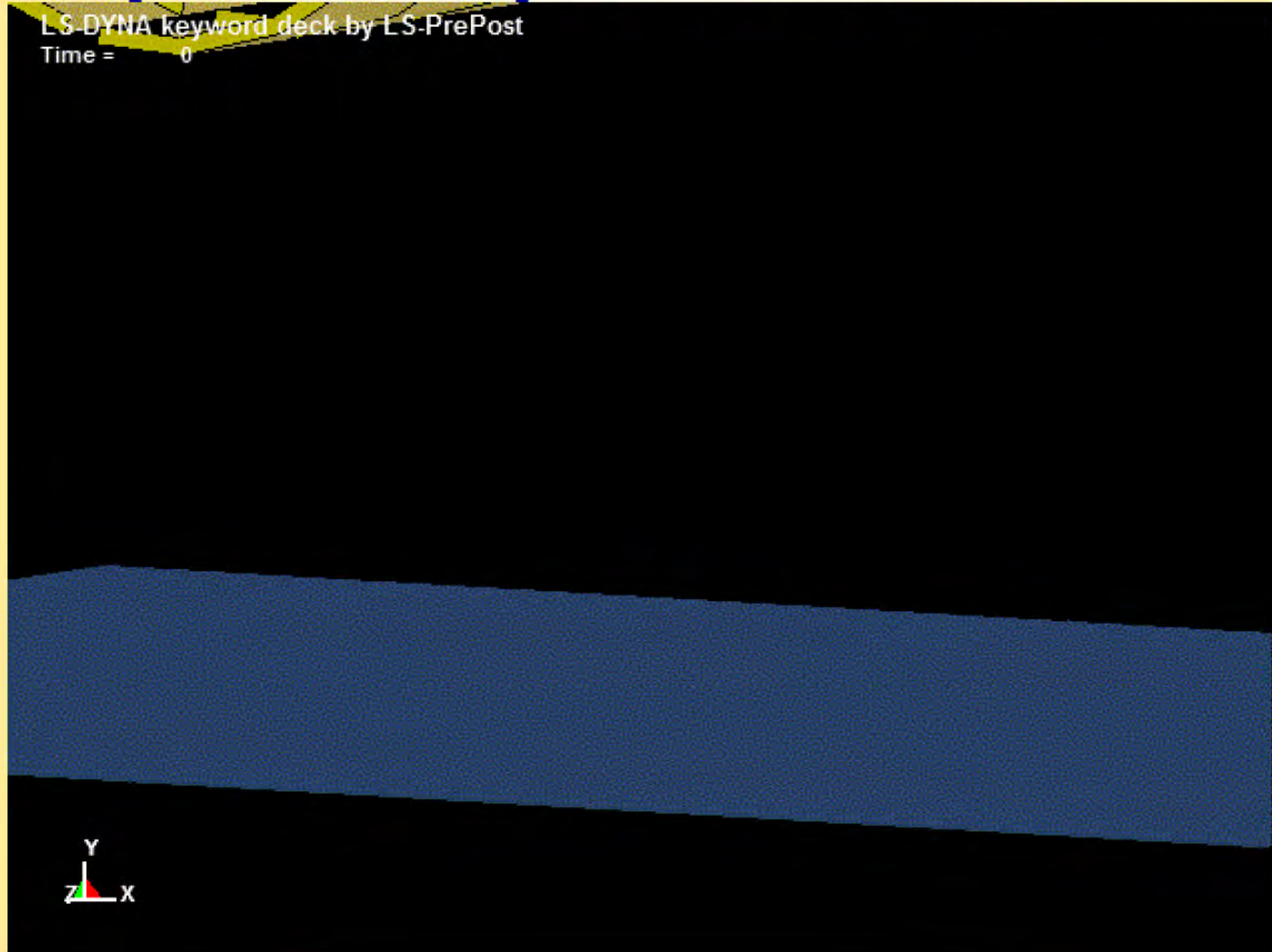
Simulation of Fuselage with Explosion Sandia National Lab – CNN 2008



Both Fuselage Walls Open Outside



Drop after Explosion in the Air



Shrapnel from Smolensk Crash Scene



State of the Art Soil Material Model Mat147 Developed by FHWA

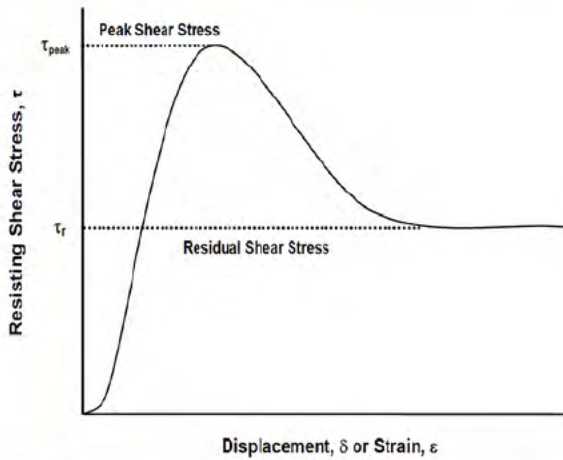


Fig.1 General direct shear performance of soil

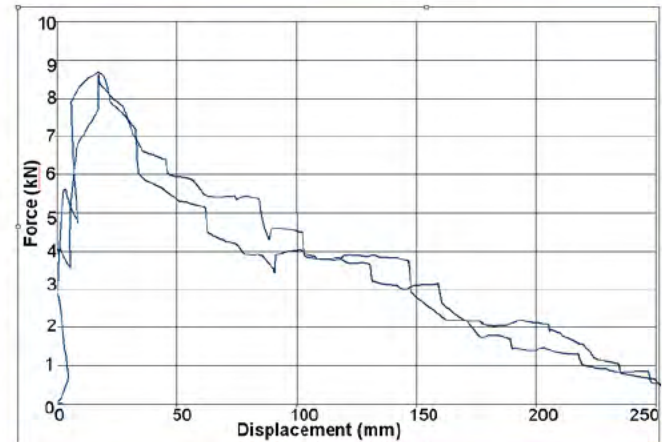
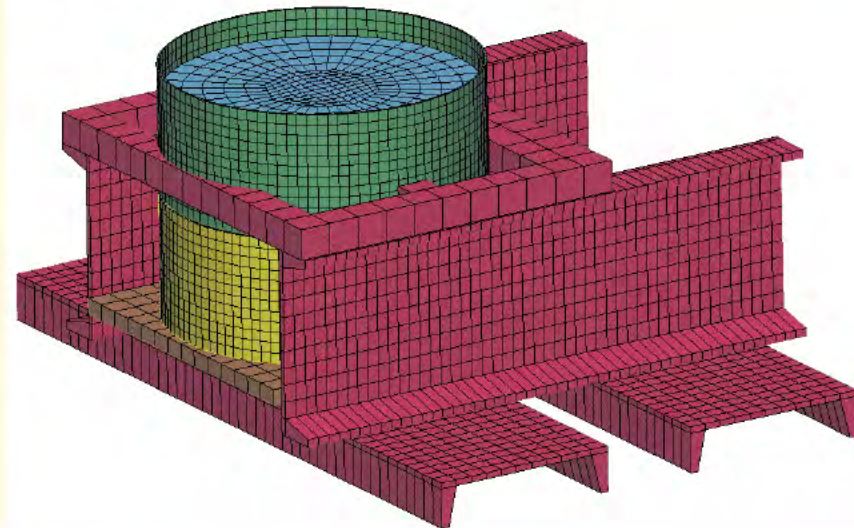


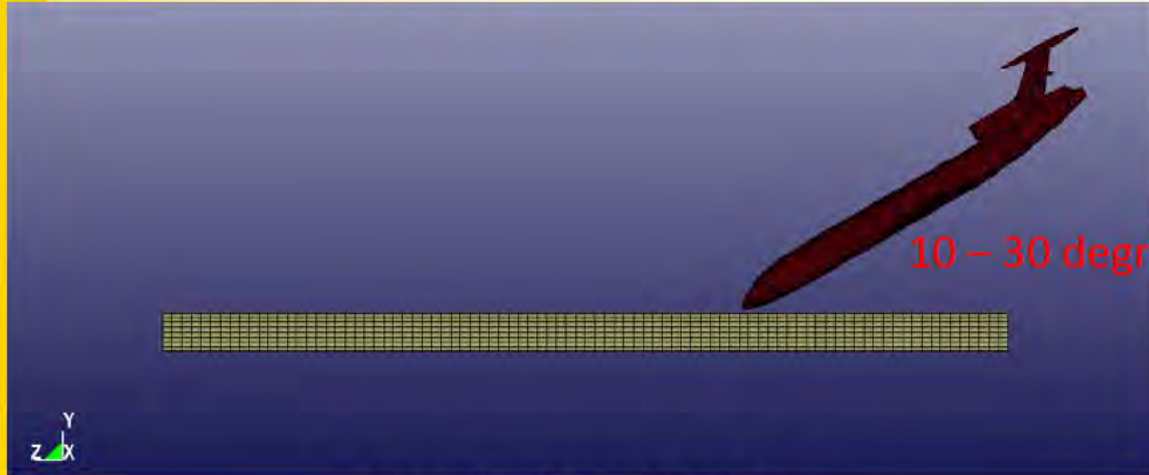
Fig.2 Results of two direct shear tests



Direct Shear Test - Baseline Model
Time = 0

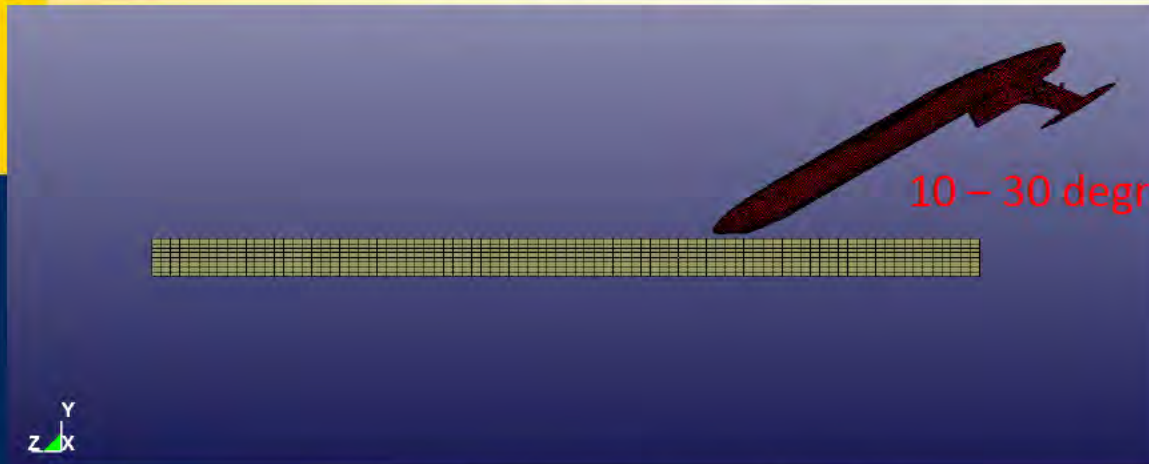


Crash Simulation using the Soil Model Mat147 in LsDyna



Regular Crash Mode

Element Size (Unit-meter):
 Ground: 1by1 in plane (x-z)
 and 0.5 thick (y) solid
 elements;
 Aircraft: 0.2by0.2 shell
 elements

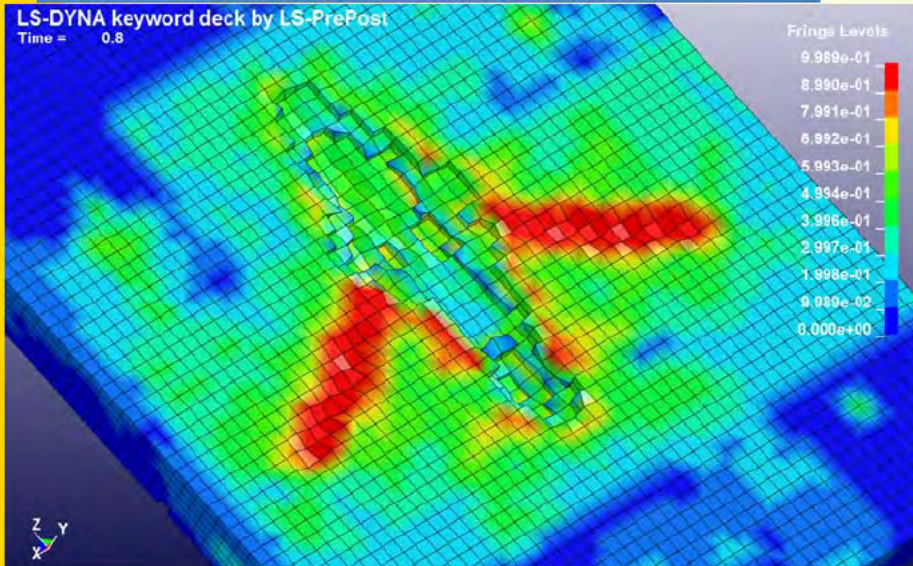


Upside down Crash Mode

Element number:
 Ground: 18304 elements;
 Plane: 32450 elements

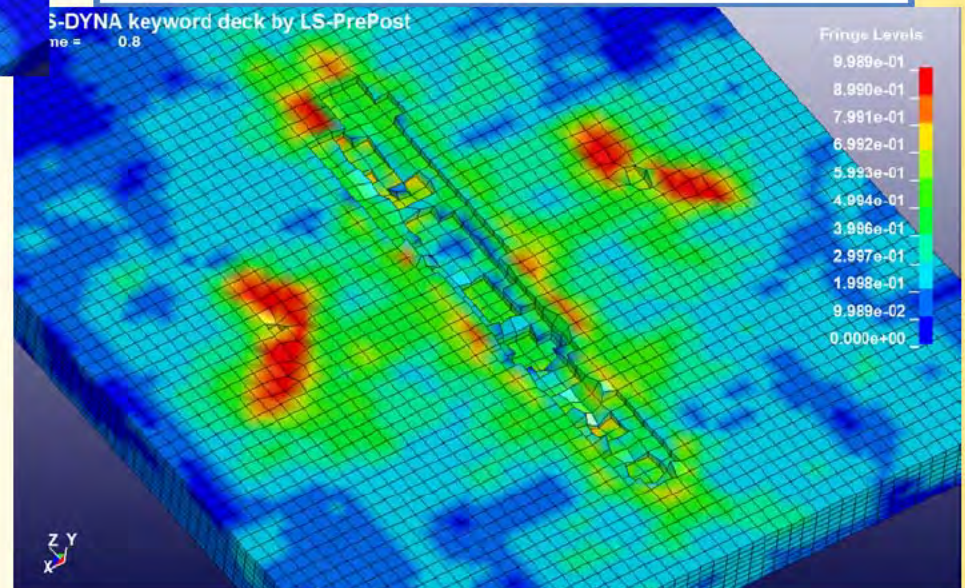
Crash Simulation 30° with Mat147

Damage Contour of Regular Case



Initial Velocity:
 Horizontal (z): 69.28 m/s;
 Vertical (y): -40 m/s

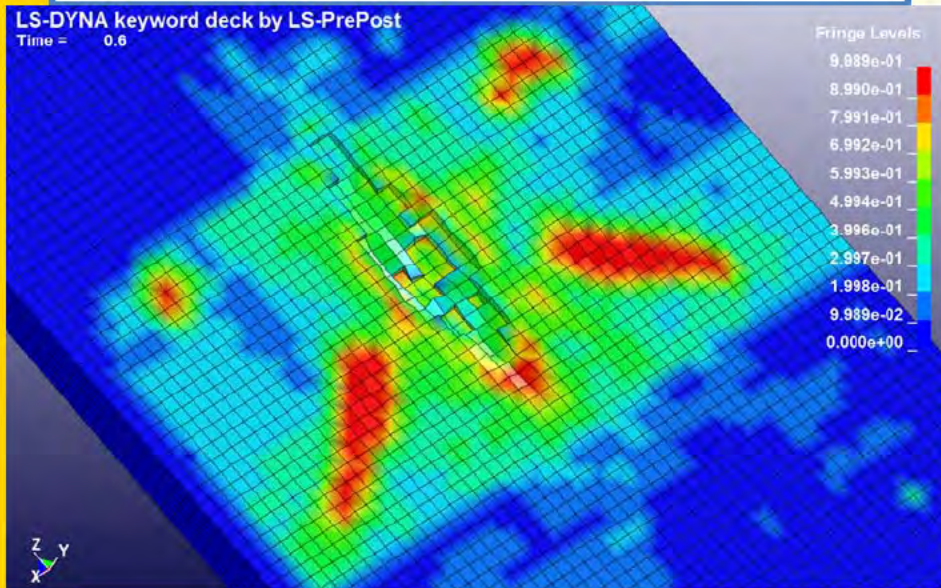
Damage Contour of Inverted Case



Crater 1-2m deep.

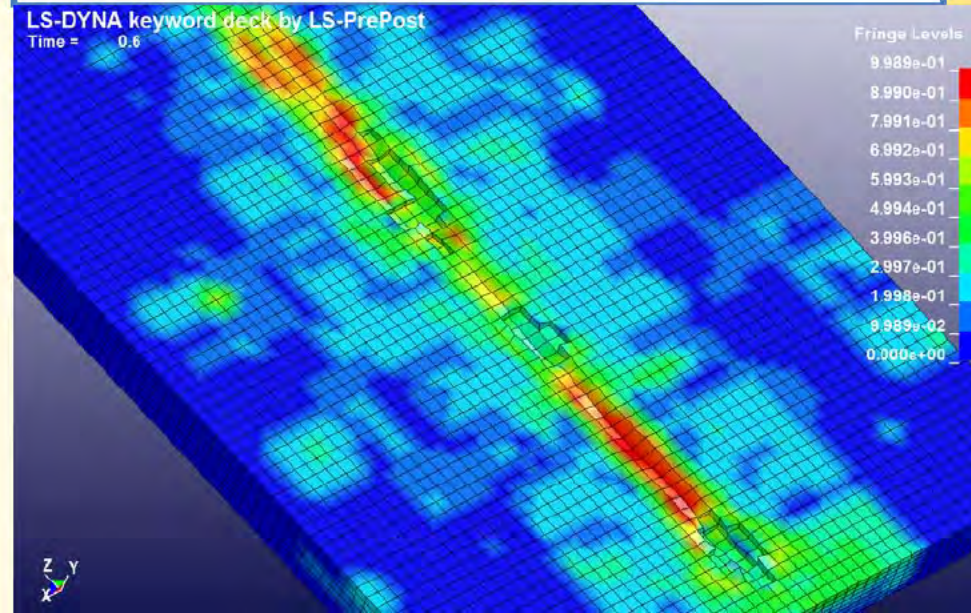
Crash Simulation 10° with Mat147

Damage Contour of regular case



Initial Velocity:
 Horizontal (z): 78.78 m/s;
 Vertical (y): -13.89 m/s

Damage Contour of Inverted Case



Conclusions Based on Soil Impact

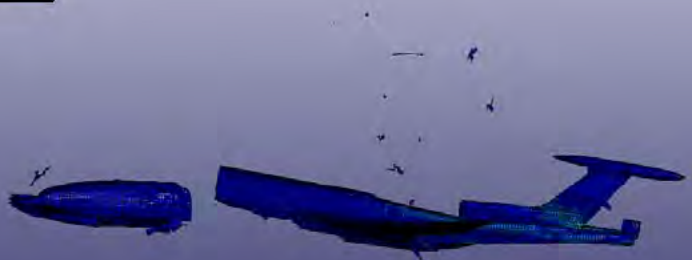
- Large and deep crater should be visible if the entire mass of the airplane was intact at the moment of the crash
- No crater detected at the scene but large field of debris suggest that the airplane disintegrated in the air



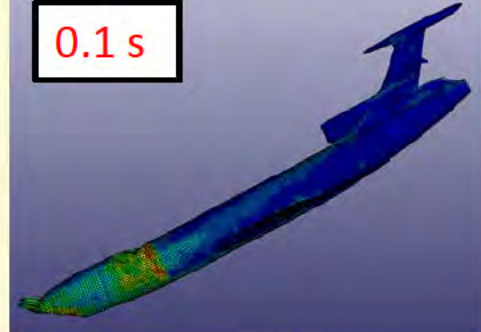
Crash Damage Process (Regular)

LS-DYNA keyword deck by LS-PrePost
Time = 0.5

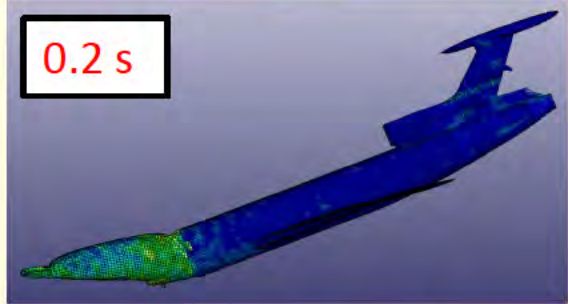
0.5 s



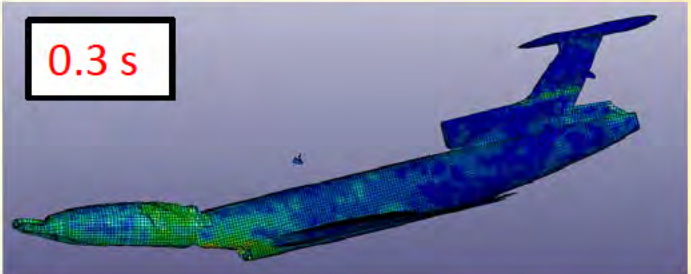
0.1 s



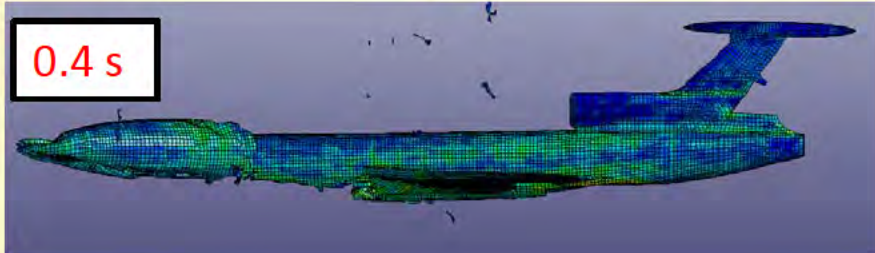
0.2 s



0.3 s



0.4 s



Boeing 727 Crash Test

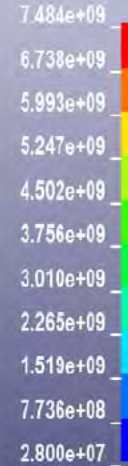


<http://dsc.discovery.com/tv-shows/curiosity/videos>

Crash Damage Process - Inverted Case

LS-DYNA keyword deck by LS-PrePost
Time = 0.5

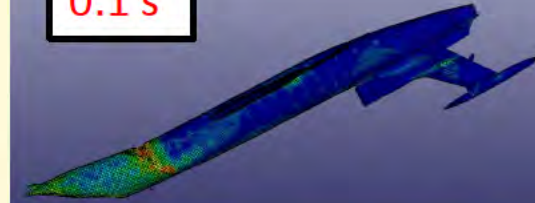
Fringe Levels



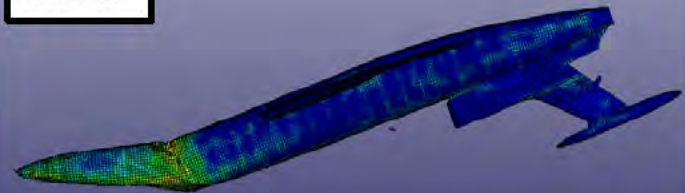
0.5 s



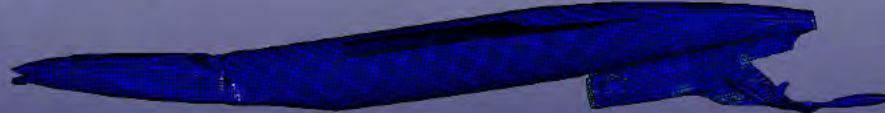
0.1 s



0.2 s



0.3 s



0.4 s



Kyrgyzstan Jet Crash (no explosion) All Survived, 31 Injured



TU-154 Airplane Crash - Dec 5, 2010

No explosion, all survived, 83 injured



Tupolev Tu-154 passenger plane belonging to Dagestan Airlines, as it crashes at Domodedovo airport in Russia
Photograph: AFP/Getty Images

Airplane Tu-154M Crash Unusually High Disintegration



Final Conclusions

- Separation of 1/3 of the left wing could not be caused by the impact with the birch tree. Most probably separation of a fragment of the left wing was caused by explosion in the air.
- Open walls outside of the fuselage indicate mid-air explosion.
- The unprecedented degree of damage and the large number of shrapnel indicate high energy mid-air explosion.
- Lack of a visible crater at the crash scene indicate that the airplane disintegrated in the mid-air.
- Without a mid-air explosion, most of the passengers in the center and aft sections of the airplane should survive any crash from 30-40 meters into the soft soil.
- Official Russian report attributed death of the passengers to 100G accelerations. Such accelerations could be explained by i) explosion in the fuselage, ii) shock wave produced by explosion, and/or iii) a direct impact of the passengers with the ground at 80m/s without any protection of the fuselage.