Smart Mater. Struct. 18 (2009) 025001 (8pp)

## A second-order theory for magnetoelectroelastic materials with transverse isotropy

W J Feng<sup>1,2</sup>, E Pan<sup>1</sup>, X Wang<sup>1</sup> and G A Gazonas<sup>3</sup>

<sup>1</sup> Department of Civil Engineering and Department of Applied Mathematics,

The University of Akron, Akron, OH 44329, USA

<sup>2</sup> Department of Engineering Mechanics, Shijiazhuang Railway Institute,

Shijiazhuang 050043, People's Republic of China

<sup>3</sup> US Army Research Laboratory, Aberdeen Proving Ground, MD 21005, USA

Received 12 March 2008, in final form 3 November 2008 Published 23 December 2008 Online at stacks.iop.org/SMS/18/025001

#### Abstract

In this paper, we concentrate on the basic governing equations of three-dimensional problems in transversely isotropic and nonlinear magnetoelectroelastic materials (i.e.,  $6\underline{m} \underline{m}$  magnetic crystals). We place emphasis on developing the nonlinear and fully coupled constitutive relations between extended traction (including elastic stress, polarization and magnetization) and extended strain (including elastic strain, electric field and magnetic induction). Simplified results are also presented for the corresponding small deformation problems in the case of both strong magnetic and electric fields and in the case of both weak magnetic and electric fields. The derived concise equations are important in investigating the nonlinear magnetoelectric effects of novel magnetoelectroelastic materials.

#### 1. Introduction

Magnetoelectroelastic materials refers to novel materials which exhibit full coupling between magnetic, electric and mechanical fields. Because of their remarkable magnetoelectric coupling effect, piezoelectric–piezomagnetic composites are potential candidates for use as magnetoelectric memory elements, smart sensors and transducers.

Van Suchtelen (1972) first reported that piezoelectricpiezomagnetic composites may exhibit a new material property—the magnetoelectric coupling effect. Later on, Van den Boomgaard *et al* (1974) and Van Run *et al* (1974) investigated the magnetoelectric effect of BaTiO<sub>3</sub>– CoFe<sub>2</sub>O<sub>4</sub> composites. In the past several decades, many achievements have been made in the micromechanical modeling of magnetoelectroelastic materials and consequently on the determination of their effective properties, especially the magnetoelectric coupling effect (Harshe *et al* 1993, Avellaneda and Harshe 1994, Li and Dunn 1998, Aboudi 2001, Srinivasan *et al* 2002, Benveniste and Milton 2003, Zheng *et al* 2004, Fiebig 2005, Nan *et al* 2005, Lin *et al* 2005).

The development of magnetoelectroelastic materials has recently stimulated the studies of some fundamental problems. These investigations include: the existence of surface waves

(Alshits et al 1992, Chen et al 2007, Liu et al 2007), wave scattering (Du et al 2004, Feng et al 2006), uniqueness and reciprocity theorems (Li 2003), various Green's function solutions (Chung and Ting 1995, Kirchner and Alshits 1996, Li 2002, Pan 2002, Wang and Shen 2002, Soh et al 2003, Lee and Ma 2007), deformation of multilayered magnetoelectroelastic plates (Pan 2001, Wang et al 2003) and circular tubes or bars (Wang and Zhong 2003), free vibration of simply supported and multilayered magnetoelectroelastic plates (Pan and Heyliger 2002), static fracture problems (Gao et al 2003a, 2003b, Song and Sih 2003, Spyropoulos et al 2003, Hu et al 2006, Wang and Mai 2007), and impact problems (Feng et al 2005, Zhou et al 2005, Feng and Su 2006). In addition, Soh and Liu (2005) derived eight types of constitutive equation for magnetoelectroelastic solids in which different independent variables were considered. The theoretical investigations mentioned above were all carried out under the assumption of linear constitutive relations.

Nonlinearity has always been an important issue in piezoelectric and magnetoelectroelastic materials/structures. While some simple nonlinear piezoelectric models were proposed to study shock waves in piezoelectric semiconductors (Lysne 1972, Chen *et al* 1976), these models are essentially semi-coupled and consequently the modeling results are

different from the experimental ones (Davison and Graham 1979). Recently, various formulations for coupled nonlinear electroelastic and magnetoelastic materials were proposed (i.e., Dorfmann and Ogden 2004, 2005; Steigmann 2004, 2008; Kankanala and Triantafyllidis 2004; Suo *et al* 2008). A review of nonlinear electroelasticity under static deformation was given by Bustamante *et al* (2008) in which different expressions for the nonlinear constitutive relations and governing equations were compared and discussed. While certain magnetoelectroelastic composites were shown to be highly nonlinear (Bichurin *et al* 2005, Nan *et al* 2008), a fully coupled nonlinear constitutive relation of them has not been developed yet.

Thus, in this paper, we derive the basic constitutive equations for three-dimensional nonlinear magnetoelectroelastic materials. The polynomial constitutive relations for a transversely isotropic (i.e.,  $6\underline{m}\underline{m}$ ) magnetic crystal are derived in a concise form using an invariant integrity basis. Furthermore the constitutive equations are fully coupled and can be specialized to the simple case of small deformation and strong magnetic and electric fields, and to the simple case of small deformation and relatively weak magnetic and electric fields. The present work should be useful to researchers in the investigation of the mechanics and physics of magnetoelectroelastic solids undergoing nonlinear deformations.

### **2.** Equations for a nonlinear magnetoelectroelastic material

Let the coordinates of a material particle with respect to a rectangular Cartesian coordinate system be  $X_K$  in the reference (undeformed) configuration and its spatial coordinates in the current (deformed) configuration be  $x_k$ . For a transversely isotropic magnetoelectroelastic material within the hexagonal system with class symmetry  $6\underline{m}\,\underline{m}$ , the basic equations for this type of nonlinear magnetoelectroelastic material can be written as follows.

#### 2.1. Governing equations

In the absence of body force, free charge density and free current density with the nonlinear magnetoelectroelastic material at rest, the balance laws and the quasistatic approximation to the Maxwell equation in the deformed configuration (lowercase subscripts) can be written as (Pao 1978, Kiral and Eringen 1990)

$$T_{kl,k} - (P_{k,k}E_l + M_{k,k}B_l) = \rho \ddot{u}_l,$$
(1)

$$(\varepsilon_0 E_k + P_k)_{,k} = 0, \tag{2}$$

$$B_{k,k} = 0, (3)$$

where  $T_{kl} = \sigma_{kl} + P_k E_l + M_k B_l$  (Pao 1978) is a symmetric stress tensor called the elastic stress,  $\sigma_{kl}$  the Cauchy stress,  $\rho$ the mass density,  $u_l$  the displacement vector,  $P_k$  the electric polarization,  $M_k$  the magnetization,  $E_k$  the electric field,  $B_k$ the magnetic induction,  $\varepsilon_0$  the permittivity of free space, and a dot above a quantity signifies its material time derivative. As shown in section 2.2, the constitutive equations are generally derived in the material (undeformed) configuration (uppercase subscripts). For the sake of application, the spatial quantities are expressed by the corresponding material ones as (Kiral and Eringen 1990, Jordan and Eringen 1964)

$$T_{kl} = J^{-1} T_{KL} x_{k,K} x_{l,L}, (4)$$

$$P_k = J^{-1} \prod_{\kappa} x_k \kappa. \tag{5}$$

$$M_k = J^{-1} M_K x_{k,K}, (6)$$

$$E_k = X_{K,k} E_K,\tag{7}$$

$$B_k = X_{K,k} B_K, (8)$$

where

$$\Pi_K = P_K / \rho, \tag{9}$$

$$J = \det(x_{k,K}) = \rho_0 / \rho, \qquad (10)$$

where  $\rho_0$  is the mass density in the material configuration; again, an uppercase subscript corresponds to the undeformed configuration, and a lowercase subscript to the deformed configuration.

#### 2.2. Constitutive equations

Modern texts in physics (Feynman *et al* 1964, Pao 1978) tend to regard the electric field (**E**) and magnetic induction (**B**) as the basic variables. The other four electromagnetic field variables, i.e. the electric displacement, polarization, magnetic field and magnetization vectors (**D**, **P**, **H**, **M**), can be related by the following two vector equations (Pao 1978):

$$\mathbf{B} = \mu_0 (\mathbf{H} + \mathbf{M}), \tag{11}$$

$$\mathbf{D} = \varepsilon_0 \mathbf{E} + \mathbf{P},\tag{12}$$

where  $\mu_0$  is the permeability of free space, which is related to  $\varepsilon_0$  by  $\mu_0\varepsilon_0 = c^{-2}$ , with *c* being the speed of light *in vacuo*.

For an isothermal or adiabatic process, in the material configuration, the free energy function in the absence of heat conduction or heat sources can be defined as (Pao 1978)

$$\Sigma = \Sigma(\Gamma_{KL}, E_K, B_K), \tag{13}$$

where  $\Gamma_{KL}$  is the Lagrangian strain (see equation (17) below).

The constitutive equations can be derived from equation (13) as (Pao 1978, Kiral and Eringen 1990)

$$T_{KL} = \frac{\partial \Sigma}{\partial \Gamma_{KL}},\tag{14}$$

$$\Pi_K = -\frac{\partial \Sigma}{\partial E_K},\tag{15}$$

$$M_K = -\frac{\partial \Sigma}{\partial B_K}.$$
 (16)

We point out that the free energy expression (13) for the general and fully coupled nonlinear magnetoelectroelastic deformation can be reduced to the simple magnetoelastic and electroelastic cases previously studied. For example, in the nonlinear magnetoelastic deformation analysis, Dorfmann and Ogden (2004) expressed the free energy in terms of the deformation gradient tensor and the magnetic field (or magnetic induction); for the nonlinear electroelastic case, the pair of the Lagrangian strain with polarization, electric field, or electric displacement could be the independent variables in the free energy expression (Bustamante *et al* 2008). It is also well known that the free energy (13) can be expressed by other triads but the work conjugates among the electric and magnetic quantities need to be carefully checked (see, e.g., Suo *et al* 2008).

# 2.3. Extended geometry equations (i.e., relations of strain–displacement, electric field–electric potential and magnetic field–magnetic potential)

In the material configuration, the Lagrangian strain, electric field, and magnetic field can be expressed as

$$\Gamma_{KL} = \frac{1}{2} (x_{k,K} x_{k,L} - \delta_{KL}) = \frac{1}{2} (u_{K,L} + u_{L,K} + u_{M,K} u_{M,L}),$$
(17)

$$E_K = -\frac{\partial \phi}{\partial X_K} = -\phi_{,K},\tag{18}$$

$$H_K = -\frac{\partial \psi}{\partial X_K} = -\psi_{,K}.$$
 (19)

Similar to equation (7), we have

$$H_k = -\frac{\partial \psi}{\partial x_k} = -\frac{\partial \psi}{\partial X_K} \frac{\partial X_K}{\partial x_k} = X_{K,k} H_K.$$
 (20)

#### 2.4. Boundary and initial conditions

(a) Mechanical boundary conditions

$$u_i = \bar{u}_i(x_1, x_2, x_3) \in S_1, \tag{21}$$

$$\sigma_{ij}n_j = \bar{p}_i(x_1, x_2, x_3) \in S_2, \tag{22}$$

where  $S_1+S_2 = S$  is the total boundary of the problem domain, and  $\bar{u}_i$  and  $\bar{p}_i$  are, respectively, the given displacement and traction on the boundary.

(b) Magnetic boundary conditions

$$\psi = \psi(x_1, x_2, x_3) \in S_3, \tag{23}$$

$$B_i n_i = B_n(x_1, x_2, x_3) \in S_4, \tag{24}$$

where  $S_3 + S_4 = S$ ,  $\bar{\psi}$  and  $\bar{B}_n$  are, respectively, the given magnetic potential and normal magnetic induction on the boundary.

(c) Electric boundary conditions

$$\phi = \phi(x_1, x_2, x_3) \in S_5, \tag{25}$$

$$D_i n_i = \bar{D}_n(x_1, x_2, x_3) \in S_6,$$
 (26)

where  $S_5 + S_6 = S$ , and  $\bar{\phi}$  and  $\bar{D}_n$  are, respectively, the given electric potential and normal electric displacement on the boundary.

(d) Initial conditions

$$u_i(x_1, x_2, x_3, 0) = u_i^0(x_1, x_2, x_3),$$
  

$$\dot{u}_i(x_1, x_2, x_3, 0) = \dot{u}_i^0(x_1, x_2, x_3),$$
(27)

where  $u_i^0$  is the known initial displacement and  $\dot{u}_i^0$  the known initial velocity within the problem domain.

### **3.** Second-order nonlinear constitutive equations of three-dimensional problems

As shown in section 2, for the nonlinear problem of concern in this paper, the nonlinear constitutive equations are the key issues. To derive these equations, we assume that the constitutive equations for stress, electric polarization and magnetization are polynomial functions of the strain, electric field and magnetic induction.

#### 3.1. Polynomial integrity basis

Two basic requirements of invariance that must be imposed upon the constitutive equations are the spatial invariance and material invariance (Jordan and Eringen 1964). For a  $6\underline{m} \underline{m}$ magnetic crystal with both the elastic symmetric axis and the poling direction as the  $X_3$ -axis, the polynomial integrity basis, the degree of which is less than three, can be given in the following concise form (Kiral and Eringen 1990).

- Elements in  $\Gamma_{IJ}$  only:
  - Degree 1:  $\Gamma_{33}$ ,  $\Gamma_{11} + \Gamma_{22}$ , (28) Degree 2:  $\Gamma_{11}\Gamma_{22} - \Gamma_{12}^2$ ,  $\Gamma_{13}^2 + \Gamma_{23}^2$ , (29) Degree 3:  $\Gamma_{11} \left( \Gamma_{11}^2 + 6\Gamma_{11}\Gamma_{22} - 12\Gamma_{12}^2 + 9\Gamma_{22}^2 \right)$ ,  $\Gamma_{11}\Gamma_{23}^2 + \Gamma_{22}\Gamma_{13}^2 - \Gamma_{13}\Gamma_{23}\Gamma_{12}$ . (30)
- Elements in  $E_I$  only:

Degree 1: 
$$E_3$$
, (31)

- Degree 2:  $E_1^2 + E_2^2$ . (32)
- Elements in  $B_I$  only:

Degree 1: 
$$B_3$$
, (33)

Degree 2: 
$$B_1^2 + B_2^2$$
. (34)

• Elements in  $\Gamma_{IJ}$  and  $E_I$  only:

Degree 2: 
$$\Gamma_{31}E_1 + \Gamma_{23}E_2$$
, (35)

Degree 3:  $(E_1\Gamma_{23} + E_2\Gamma_{31})\Gamma_{12} - E_1\Gamma_{22}\Gamma_{31} - E_2\Gamma_{11}\Gamma_{23}$ ,

$$\Gamma_{11}E_2^2 + \Gamma_{22}E_1^2 - 2E_1E_2\Gamma_{12}.$$
 (36*a*)  
(36*b*)

- Elements in  $\Gamma_{IJ}$  and  $B_I$  only:
  - Degree 2:  $\Gamma_{31}B_1 + \Gamma_{23}B_2$ , (37)

Degree 3:  $(B_1\Gamma_{23} + B_2\Gamma_{31})\Gamma_{12} - B_1\Gamma_{22}\Gamma_{31} - B_2\Gamma_{11}\Gamma_{23},$ (38*a*)  $\Gamma_{11}B_2^2 + \Gamma_{22}B_1^2 - 2B_1B_2\Gamma_{12}.$  (38*b*)

- $\mathbf{1}_{11}\mathbf{D}_2 + \mathbf{1}_{22}\mathbf{D}_1 2\mathbf{D}_1\mathbf{D}_2\mathbf{1}_{12}.$  (5)
- Elements in  $E_I$  and  $B_I$  only:
  - Degree 2:  $E_1B_1 + E_2B_2$ . (39)
- Elements in  $\Gamma_{IJ}$ ,  $E_I$  and  $B_I$  only:

Degree 3: 
$$\operatorname{Im}\{(B_1 + iB_2)(E_1 + iE_2) \times [2\Gamma_{12} + i(\Gamma_{11} - \Gamma_{22})]\}.$$
 (40)

#### 3.2. Polynomial free energy function

In order to derive the second-order nonlinear constitutive equations, the free energy  $\Sigma$  should be formed as a thirdorder polynomial function of  $\Gamma_{IJ}$ ,  $E_I$  and  $B_I$  (Yang and Betra 1995). From equations (28) to (40), after complicated symbolic mathematical manipulations using the *Mathematica* software package, the free energy  $\Sigma$  can be finally expressed in the following form:

$$\Sigma = \Sigma_a + \Sigma_b + \Sigma_c + \Sigma_d + \Sigma_s + \Sigma_f + \Sigma_g, \qquad (41)$$

where

$$\begin{split} \Sigma_{a} &= a_{1}\Gamma_{33} + a_{2}(\Gamma_{11} + \Gamma_{22}) + a_{3}(\Gamma_{11}\Gamma_{22} - \Gamma_{12}^{2}) \\ &+ a_{4}(\Gamma_{23}^{2} + \Gamma_{31}^{2}) + a_{5}\Gamma_{33}^{2} + a_{6}(\Gamma_{11} + \Gamma_{22})\Gamma_{33} \\ &+ a_{7}(\Gamma_{11} + \Gamma_{22})^{2} + a_{8}\Gamma_{11}(\Gamma_{11}^{2} - 12\Gamma_{12}^{2} + 6\Gamma_{11}\Gamma_{22} \\ &+ 9\Gamma_{22}^{2}) + a_{9}(\Gamma_{11}\Gamma_{23}^{2} + \Gamma_{31}(\Gamma_{22}\Gamma_{31} - \Gamma_{12}\Gamma_{23})) \\ &+ a_{10}(\Gamma_{11}\Gamma_{22} - \Gamma_{12}^{2})\Gamma_{33} + a_{11}(\Gamma_{23}^{2} + \Gamma_{31}^{2})\Gamma_{33} \\ &+ a_{12}(\Gamma_{11} + \Gamma_{22})(\Gamma_{11}\Gamma_{22} - \Gamma_{12}^{2}) \\ &+ a_{13}(\Gamma_{11} + \Gamma_{22})(\Gamma_{23}^{2} + \Gamma_{31}^{2}) + a_{14}\Gamma_{33}^{3} \\ &+ a_{15}(\Gamma_{11} + \Gamma_{22})\Gamma_{33}^{2} + a_{16}(\Gamma_{11} + \Gamma_{22})^{3} \\ &+ a_{17}(\Gamma_{11} + \Gamma_{22})^{2}\Gamma_{33}, \end{split}$$
(42a) 
$$\Sigma_{b} &= b_{1}E_{3} + b_{2}(E_{1}^{2} + E_{2}^{2}) + b_{3}E_{3}^{2} + b_{4}(E_{1}^{2} + E_{2}^{2})E_{3} \\ &+ b_{5}E_{3}^{3}. \end{split}$$

$$\Sigma_{c} = c_{1}B_{3} + c_{2}(B_{1}^{2} + B_{2}^{2}) + c_{3}B_{3}^{2} + c_{4}(B_{1}^{2} + B_{2}^{2})B_{3} + c_{5}B_{3}^{3}, \qquad (42c)$$

$$\begin{split} \Sigma_{d} &= d_{1}(\Gamma_{31}E_{1} + \Gamma_{23}E_{2}) + d_{2}\Gamma_{33}E_{3} + d_{3}(\Gamma_{11} + \Gamma_{22})E_{3} \\ &+ d_{4}(\Gamma_{12}\Gamma_{23}E_{1} - \Gamma_{22}\Gamma_{31}E_{1} - \Gamma_{11}\Gamma_{23}E_{2} + \Gamma_{12}\Gamma_{31}E_{2}) \\ &+ d_{5}\Gamma_{33}(\Gamma_{31}E_{1} + \Gamma_{23}E_{2}) + d_{6}(\Gamma_{11} + \Gamma_{22})(\Gamma_{31}E_{1} \\ &+ \Gamma_{23}E_{2}) + d_{7}(-\Gamma_{12}^{2} + \Gamma_{11}\Gamma_{22})E_{3} + d_{8}(\Gamma_{23}^{2} + \Gamma_{31}^{2})E_{3} \\ &+ d_{9}\Gamma_{33}^{2}E_{3} + d_{10}(\Gamma_{11} + \Gamma_{22})^{2}E_{3} + d_{11}(\Gamma_{11} + \Gamma_{22})\Gamma_{33}E_{3} \\ &+ d_{12}(\Gamma_{22}E_{1}^{2} + E_{2}(-2\Gamma_{12}E_{1} + \Gamma_{11}E_{2})) + d_{13}\Gamma_{33}(E_{1}^{2} \\ &+ E_{2}^{2}) + d_{14}(\Gamma_{11} + \Gamma_{22})(E_{1}^{2} + E_{2}^{2}) \\ &+ d_{15}(\Gamma_{31}E_{1} + \Gamma_{23}E_{2})E_{3} + d_{16}\Gamma_{33}E_{3}^{2} \\ &+ d_{17}(\Gamma_{11} + \Gamma_{22})E_{3}^{2}, \end{split}$$

$$\begin{split} \Sigma_{s} &= s_{1}(\Gamma_{31}B_{1} + \Gamma_{23}B_{2}) + s_{2}\Gamma_{33}B_{3} + s_{3}(\Gamma_{11} + \Gamma_{22})B_{3} \\ &+ s_{4}(\Gamma_{12}\Gamma_{23}B_{1} - \Gamma_{22}\Gamma_{31}B_{1} - \Gamma_{11}\Gamma_{23}B_{2} + \Gamma_{12}\Gamma_{31}B_{2}) \\ &+ s_{5}\Gamma_{33}(\Gamma_{31}B_{1} + \Gamma_{23}B_{2}) + s_{6}(\Gamma_{11} + \Gamma_{22})(\Gamma_{31}B_{1} \\ &+ \Gamma_{23}B_{2}) + s_{7}(-\Gamma_{12}^{2} + \Gamma_{11}\Gamma_{22})B_{3} + s_{8}(\Gamma_{23}^{2} + \Gamma_{31}^{2})B_{3} \\ &+ s_{9}\Gamma_{33}^{2}B_{3} + s_{10}(\Gamma_{11} + \Gamma_{22})^{2}B_{3} + s_{11}(\Gamma_{11} + \Gamma_{22})\Gamma_{33}B_{3} \\ &+ s_{12}(\Gamma_{22}B_{1}^{2} + B_{2}(-2\Gamma_{12}B_{1} + \Gamma_{11}B_{2})) + s_{13}\Gamma_{33}(B_{1}^{2} \\ &+ B_{2}^{2}) + s_{14}(\Gamma_{11} + \Gamma_{22})(B_{1}^{2} + B_{2}^{2}) \\ &+ s_{15}(\Gamma_{31}B_{1} + \Gamma_{23}B_{2})B_{3} + s_{16}\Gamma_{33}B_{3}^{2} \\ &+ s_{17}(\Gamma_{11} + \Gamma_{22})B_{3}^{2}, \end{split}$$
(42e) 
$$\Sigma_{f} &= f_{1}(B_{1}E_{1} + B_{2}E_{2}) + f_{2}B_{3}E_{3} + f_{3}(B_{1}^{2} + B_{2}^{2})E_{3} \end{split}$$

$$+ f_{4}B_{3}(B_{1}E_{1} + B_{2}E_{2}) + f_{5}B_{3}^{2}E_{3} + f_{6}(B_{1}E_{1} + B_{2}E_{2})E_{3} + f_{7}B_{3}(E_{1}^{2} + E_{2}^{2}) + f_{8}B_{3}E_{3}^{2},$$

$$\Sigma_{g} = g_{1}(2\Gamma_{12}(B_{2}E_{1} + B_{1}E_{2}) + (\Gamma_{11} - \Gamma_{22})(B_{1}E_{1} - B_{2}E_{2})) + g_{2}\Gamma_{33}(B_{1}E_{1} + B_{2}E_{2}) + g_{3}(\Gamma_{11} + \Gamma_{22})$$

$$(42f)$$

$$\times (B_1 E_1 + B_2 E_2) + g_4 (\Gamma_{31} B_1 + \Gamma_{23} B_2) E_3 + g_5 B_3 (\Gamma_{31} E_1 + \Gamma_{23} E_2) + g_6 \Gamma_{33} B_3 E_3 + g_7 (\Gamma_{11} + \Gamma_{22}) B_3 E_3.$$
(42g)

Equation (42) indicates that the free energy consists of seven parts with  $\Sigma_a$ ,  $\Sigma_b$ ,  $\Sigma_c$ ,  $\Sigma_d$ ,  $\Sigma_s$ ,  $\Sigma_f$  and  $\Sigma_g$  corresponding, respectively, to the purely mechanical properties, purely electric properties, purely magnetic properties, electromechanical coupling properties, magnetomechanical coupling properties, magnetoelectric coupling properties and magnetoelectromechanical coupling properties. It is also observed that there are a total of 76 independent material constants for a 6<u>m m</u> magnetic crystal and that there are 21 independent constants for the corresponding linearized material.

#### 3.3. Second-order constitutive theory

Substituting equations (41) and (42) into equations (14)–(16), we can express the elastic stresses, polarization and magnetization as follows:

$$T_{IJ} = T_{IJa} + T_{IJd} + T_{IJs} + T_{IJg}, (43)$$

$$\Pi_{I} = \Pi_{Ib} + \Pi_{Id} + \Pi_{If} + \Pi_{Ig}, \tag{44}$$

$$M_I = M_{Ic} + M_{Is} + M_{If} + M_{Ig}, (45)$$

where

$$T_{11a} = a_2 + a_3\Gamma_{22} + a_6\Gamma_{33} + 2a_7(\Gamma_{11} + \Gamma_{22}) + 3a_8(\Gamma_{11}^2 - 4\Gamma_{12}^2 + 4\Gamma_{11}\Gamma_{22} + 3\Gamma_{22}^2) + a_9\Gamma_{23}^2 + a_{10}\Gamma_{22}\Gamma_{33} + a_{12}(-\Gamma_{12}^2 + 2\Gamma_{11}\Gamma_{22} + \Gamma_{22}^2) + a_{13}(\Gamma_{23}^2 + \Gamma_{31}^2) + a_{15}\Gamma_{33}^2 - 3a_{16}(\Gamma_{11} + \Gamma_{22})^2 + 2a_{17}(\Gamma_{11} + \Gamma_{22})\Gamma_{33},$$
(46a)

$$T_{11d} = d_3 E_3 - d_4 \Gamma_{23} E_2 + d_6 (\Gamma_{31} E_1 + \Gamma_{23} E_2) + d_7 \Gamma_{22} E_3 + 2d_{10} (\Gamma_{11} + \Gamma_{22}) E_3 + d_{11} \Gamma_{33} E_3 + d_{12} E_2^2 + d_{14} (E_1^2 + E_2^2) + d_{17} E_3^2,$$
(46b)

$$T_{11s} = s_3 B_3 - s_4 \Gamma_{23} B_2 + s_6 (\Gamma_{31} B_1 + \Gamma_{23} B_2) + s_7 \Gamma_{22} B_3 + 2s_{10} (\Gamma_{11} + \Gamma_{22}) B_3 + s_{11} \Gamma_{33} B_3 + s_{12} B_2^2 + s_{14} (B_1^2 + B_2^2) + s_{17} B_3^2,$$
(46c)

$$T_{11g} = g_1(B_1E_1 - B_2E_2) + g_3(B_1E_1 + B_2E_2) + g_7B_3E_3,$$
(46d)

$$T_{22a} = a_2 + a_3\Gamma_{11} + a_6\Gamma_{33} + 2a_7(\Gamma_{11} + \Gamma_{22}) + 6a_8\Gamma_{11}(\Gamma_{11} + 3\Gamma_{22}) + a_9\Gamma_{31}^2 + a_{10}\Gamma_{11}\Gamma_{33} + a_{12}(-\Gamma_{12}^2 + 2\Gamma_{11}\Gamma_{22} + \Gamma_{11}^2) + a_{13}(\Gamma_{23}^2 + \Gamma_{31}^2) + a_{15}\Gamma_{33}^2 + 3a_{16}(\Gamma_{11} + \Gamma_{22})^2 + a_{17}(\Gamma_{11} + \Gamma_{22})\Gamma_{33},$$
(47*a*)

$$T_{22d} = d_3 E_3 - d_4 \Gamma_{31} E_1 + d_6 (\Gamma_{31} E_1 + \Gamma_{23} E_2) + d_7 \Gamma_{11} E_3 + 2d_{10} (\Gamma_{11} + \Gamma_{22}) E_3 + d_{11} \Gamma_{33} E_3 + d_{12} E_1^2 + d_{14} (E_1^2 + E_2^2) + d_{17} E_3^2,$$
(47b)

$$T_{22s} = s_3 B_3 - s_4 \Gamma_{31} B_1 + s_6 (\Gamma_{31} B_1 + \Gamma_{23} B_2) + s_7 \Gamma_{11} B_3 + 2s_{10} (\Gamma_{11} + \Gamma_{22}) B_3 + s_{11} \Gamma_{33} B_3 + s_{12} B_1^2 + s_{14} (B_1^2 + B_2^2) + s_{17} B_3^2,$$
(47c)

$$T_{22g} = g_1(-B_1E_1 + B_2E_2) + g_3(B_1E_1 + B_2E_2) + g_7B_3E_3,$$
(47d)

$\overline{T_{33a}} = a_1 + 2a_5\Gamma_{33} + a_6(\Gamma_{11} + \Gamma_{22}) + a_{10}(-\Gamma_{12}^2 + \Gamma_{11})$	Γ <sub>22</sub> )
$+a_{11}(\Gamma_{23}^2+\Gamma_{31}^2)+3a_{14}\Gamma_{33}^2+2a_{15}(\Gamma_{11}+\Gamma_{22})\Gamma_{33}$	
$+a_{17}(\Gamma_{11}+\Gamma_{22})^2,$	(48 <i>a</i> )
$T_{33d} = d_2 E_3 + d_5 (\Gamma_{31} E_1 + \Gamma_{23} E_2) + 2d_9 \Gamma_{33} E_3$	
$+ d_{11}(\Gamma_{11} + \Gamma_{22})E_3 + d_{13}(E_1^2 + E_2^2) + d_{16}E_3^2,$	(48 <i>b</i> )
$T_{33s} = s_2 B_3 + s_5 (\Gamma_{31} B_1 + \Gamma_{23} B_2) + 2s_9 \Gamma_{33} B_3$	
$+ s_{11}(\Gamma_{11} + \Gamma_{22})B_3 + s_{13}(B_1^2 + B_2^2) + s_{16}B_3^2,$	(48 <i>c</i> )
$T_{33g} = g_2 \left( B_1 E_1 + B_2 E_2 \right) + g_6 B_3 E_3,$	(48 <i>d</i> )
$T_{23a} = a_4 \Gamma_{23} + a_9 (\Gamma_{11} \Gamma_{23} - 0.5 \Gamma_{12} \Gamma_{31}) + a_{11} \Gamma_{23} \Gamma_{33}$	
$+a_{13}(\Gamma_{11}+\Gamma_{22})\Gamma_{23},$	(49 <i>a</i> )
$T_{23d} = 0.5d_1E_2 + 0.5d_4(\Gamma_{12}E_1 - \Gamma_{11}E_2) + 0.5d_5\Gamma_{33}E_2$	2
$+ 0.5d_6(\Gamma_{11} + \Gamma_{22})E_2 + d_8\Gamma_{23}E_3 + 0.5d_{15}E_2E_3,$	(49 <i>b</i> )
$T_{23s} = 0.5s_1B_2 + 0.5s_4(\Gamma_{12}B_1 - \Gamma_{11}B_2) + 0.5s_5\Gamma_{33}B_2$	
$+ 0.5s_6(\Gamma_{11} + \Gamma_{22})B_2 + s_8\Gamma_{23}B_3 + 0.5s_{15}B_2B_3,$	(49 <i>c</i> )
$T_{23g} = 0.5g_4B_2E_3 + 0.5g_5B_3E_2,$	(49 <i>d</i> )
$T_{31a} = a_4 \Gamma_{31} + a_9 (\Gamma_{22} \Gamma_{31} - 0.5 \Gamma_{12} \Gamma_{23}) + a_{11} \Gamma_{31} \Gamma_{33}$	
$+a_{13}(\Gamma_{11}+\Gamma_{22})\Gamma_{31},$	(50 <i>a</i> )
$T_{31d} = 0.5d_1E_1 + 0.5d_4(\Gamma_{12}E_2 - \Gamma_{22}E_1) + 0.5d_5\Gamma_{33}E_1$	1
$+ 0.5d_6(\Gamma_{11} + \Gamma_{22})E_1 + d_8\Gamma_{31}E_3 + 0.5d_{15}E_1E_3,$	(50 <i>b</i> )
$T_{31s} = 0.5s_1B_1 + 0.5s_4(\Gamma_{12}B_2 - \Gamma_{22}B_1) + 0.5s_5\Gamma_{33}B_1$	
$+0.5s_6(\Gamma_{11}+\Gamma_{22})B_1+s_8\Gamma_{31}B_3+0.5s_{15}B_1B_3,$	(50 <i>c</i> )
$T_{31g} = 0.5g_4B_1E_3 + 0.5g_5B_3E_1,$	(50d)
$T_{12a} = -a_3\Gamma_{12} - 12a_8\Gamma_{11}\Gamma_{12} - 0.5a_9\Gamma_{23}\Gamma_{31} - a_{10}\Gamma_{12}\Gamma_{12}$	33
$-a_{12}\Gamma_{12}(\Gamma_{11}+\Gamma_{12}),$	(51 <i>a</i> )
$T_{12d} = 0.5d_4(\Gamma_{23}E_1 + \Gamma_{31}E_2) - d_7\Gamma_{12}E_3 - d_{12}E_1E_2,$	(51 <i>b</i> )
$T_{12s} = 0.5s_4(\Gamma_{23}B_1 + \Gamma_{31}B_2) - s_7\Gamma_{12}B_3 - s_{12}B_1B_2,$	(51 <i>c</i> )
$T_{12g} = g_1(B_2E_1 + B_1E_2),$	(51 <i>d</i> )
$-\Pi_{1b} = 2b_2E_1 + 2b_4E_1E_3,$	(52 <i>a</i> )
$-\Pi_{1d} = d_1\Gamma_{31} + d_4(\Gamma_{12}\Gamma_{23} - \Gamma_{22}\Gamma_{31}) + d_5\Gamma_{31}\Gamma_{33}$	
$+ d_6(\Gamma_{11} + \Gamma_{22})\Gamma_{31} + 2d_{12}(\Gamma_{22}E_1 - \Gamma_{12}E_2)$	
$+ 2d_{13}\Gamma_{33}E_1 + 2d_{14}(\Gamma_{11} + \Gamma_{22})E_1 + d_{15}\Gamma_{31}E_3,$	(52 <i>b</i> )
$-\Pi_{1f} = f_1 B_1 + f_4 B_1 B_3 + f_6 B_1 E_3 + 2f_7 B_3 E_1,$	(52 <i>c</i> )
$-\Pi_{1g} = g_1((\Gamma_{11} - \Gamma_{22})B_1 + 2\Gamma_{12}B_2) + g_2\Gamma_{33}B_1$	
$+g_3(\Gamma_{11}+\Gamma_{22})B_1+g_5\Gamma_{31}B_3,$	(52 <i>d</i> )
$-\Pi_{2b} = 2b_2E_2 + 2b_4E_2E_3,$	(53 <i>a</i> )
$-\Pi_{2d} = d_1\Gamma_{23} + d_4(-\Gamma_{11}\Gamma_{23} + \Gamma_{12}\Gamma_{31}) + d_5\Gamma_{23}\Gamma_{33}$	
$+ d_6(\Gamma_{11} + \Gamma_{22})\Gamma_{23} + 2d_{12}(-\Gamma_{12}E_1 + \Gamma_{11}E_2)$	
$+ 2d_{13}\Gamma_{33}E_2 + 2d_{14}(\Gamma_{11} + \Gamma_{22})E_2 + d_{15}\Gamma_{23}E_3,$	(53 <i>b</i> )
$-\Pi_{2f} = f_1 B_2 + f_4 B_2 B_3 + f_6 B_2 E_3 + 2f_7 B_3 E_2,$	(53 <i>c</i> )
$-\Pi_{2g} = g_1((\Gamma_{22} - \Gamma_{11})B_2 + 2\Gamma_{12}B_1) + g_2\Gamma_{33}B_2$	
$+g_3(\Gamma_{11}+\Gamma_{22})B_2+g_5\Gamma_{23}B_3,$	(53 <i>d</i> )

$$-\Pi_{3b} = b_1 + 2b_3E_3 + b_4(E_1^2 + E_2^2) + 3b_5E_3^2,$$
(54*a*)

$$-\Pi_{3d} = d_2\Gamma_{33} + d_3(\Gamma_{11} + \Gamma_{22}) + d_7(-\Gamma_{12}^2 + \Gamma_{11}\Gamma_{22}) + d_8(\Gamma_{23}^2 + \Gamma_{31}^2) + d_9\Gamma_{33}^2 + d_{10}(\Gamma_{11} + \Gamma_{22})^2$$

$$+ d_{11}(\Gamma_{11} + \Gamma_{22})\Gamma_{33} + d_{15}(\Gamma_{31}E_1 + \Gamma_{23}E_2) + 2d_{16}\Gamma_{33}E_3 + 2d_{17}(\Gamma_{11} + \Gamma_{22})E_3,$$
(54b)

$$-\Pi_{3f} = f_2 B_3 + f_3 (B_1^2 + B_2^2) + f_5 B_3^2 + f_6 (B_1 E_1 + B_2 E_2) + 2f_8 B_3 E_3,$$
(54c)

$$-\Pi_{3g} = g_4(\Gamma_{31}B_1 + \Gamma_{23}B_2) + g_6\Gamma_{33}B_3 + g_7(\Gamma_{11} + \Gamma_{22})B_3,$$
(54d)

$$-M_{1c} = 2c_2B_1 + 2c_4B_1B_3, (55a)$$

$$-M_{1s} = s_1\Gamma_{31} + s_4(\Gamma_{12}\Gamma_{23} - \Gamma_{22}\Gamma_{31}) + s_5\Gamma_{31}\Gamma_{33} + s_6(\Gamma_{11} + \Gamma_{22})\Gamma_{31} + 2s_{12}(\Gamma_{22}B_1 - \Gamma_{12}B_2)$$

$$+2s_{13}\Gamma_{33}B_1+2s_{14}(\Gamma_{11}+\Gamma_{22})B_1+s_{15}\Gamma_{31}B_3, \quad (55b)$$

$$-M_{1f} = J_1 E_1 + 2J_3 B_1 E_3 + J_4 B_3 E_1 + J_6 E_1 E_3, \qquad (55c)$$
$$-M_{c} = g_{c} ((\Gamma_{cc} - \Gamma_{cc}) E_1 + 2\Gamma_{cc} E_2) + g_{c} \Gamma_{cc} E_2$$

$$-m_{1g} = g_1((\Gamma_{11} - \Gamma_{22})E_1 + 2\Gamma_{12}E_2) + g_2\Gamma_{33}E_1 + g_3(\Gamma_{11} + \Gamma_{22})E_1 + g_4\Gamma_{31}E_3,$$
(55d)

$$-M_{2c} = 2c_2B_2 + 2c_4B_2B_3, (56a)$$

$$-M_{2s} = s_1\Gamma_{23} + s_4(\Gamma_{12}\Gamma_{31} - \Gamma_{11}\Gamma_{23}) + s_5\Gamma_{23}\Gamma_{33} + s_6(\Gamma_{11} + \Gamma_{22})\Gamma_{23} + 2s_{12}(\Gamma_{11}B_2 - \Gamma_{12}B_1) + 2s_{13}\Gamma_{33}B_2 + 2s_{14}(\Gamma_{11} + \Gamma_{22})B_2 + s_{15}\Gamma_{23}B_3,$$
(56b)

$$M_{2f} = f_1 E_2 + 2f_3 B_2 E_3 + f_4 B_3 E_2 + f_6 E_2 E_3,$$
(56c)

$$-M_{2g} = g_1((\Gamma_{22} - \Gamma_{11})E_2 + 2\Gamma_{12}E_1) + g_2\Gamma_{33}E_2 + g_3(\Gamma_{11} + \Gamma_{22})E_2 + g_4\Gamma_{23}E_3,$$
(56d)

$$-M_{3c} = c_1 + 2c_3B_3 + c_4(B_1^2 + B_2^2) + 3c_5B_3^2,$$
(57*a*)

$$-M_{3s} = s_2\Gamma_{33} + s_3(\Gamma_{11} + \Gamma_{22}) + s_7(-\Gamma_{12}^2 + \Gamma_{11}\Gamma_{22}) + s_8(\Gamma_{23}^2 + \Gamma_{31}^2) + s_9\Gamma_{33}^2 + s_{10}(\Gamma_{11} + \Gamma_{22})^2 + s_{11}(\Gamma_{11} + \Gamma_{22})\Gamma_{33} + s_{15}(\Gamma_{31}B_1 + \Gamma_{23}B_2) + 2s_{16}\Gamma_{33}B_3 + 2s_{17}(\Gamma_{11} + \Gamma_{22})B_3,$$
(57b)  
$$-M_{2s} = f_sF_s + f_s(B_sF_s + B_sF_s) + 2f_sB_sF_s$$

$$-M_{3f} = f_2 E_3 + f_4 (B_1 E_1 + B_2 E_2) + 2f_5 B_3 E_3 + f_7 (E_1^2 + E_2^2) + f_8 E_3^2,$$
(57c)

$$-M_{3g} = g_5(\Gamma_{31}E_1 + \Gamma_{23}E_2) + g_6\Gamma_{33}E_3 + g_7(\Gamma_{11} + \Gamma_{22})E_3.$$
(57d)

Equations (46*a*), (47*a*), (48*a*), (54*a*) and (57*a*) imply that  $a_2$  and  $a_1$  correspond to the initial stresses,  $b_1$  to the initial polarization, and  $c_1$  to the initial magnetization. Thus, if the magnetoelectroelastic medium considered here is in a free state, there are, in fact, only 72 independent material constants for the nonlinear magnetoelectroelastic material.

Therefore, we have derived the concise expressions of the nonlinear fully coupled constitutive equations for a  $6\underline{m} \underline{m}$  magnetic crystal. While our results should be the foundation of future numerical analysis on the nonlinear problems of magnetoelectroelastic materials, the correctness of these equations can be further verified indirectly by reducing them to different special cases. We discuss two special cases below.

### 4. Small deformation but strong magnetic and electric fields

Let us assume that the magnetoelectroelastic domain is under a small deformation but with strong magnetic and electric fields. Then, there is no difference between the Lagrangian and Eulerian strains. In other words,

$$\Gamma_{KL} = \frac{1}{2}(u_{K,L} + u_{L,K}) \equiv \overline{\Gamma}_{KL}.$$
(58)

If all the quadratic terms with respect to  $\Gamma_{KL}(\overline{\Gamma}_{KL})$  are dropped, we can directly obtain, from section 3, the constitutive equations corresponding to small deformation but strong magnetic and electric fields.

In this case, the Lagrangian strain  $\Gamma_{KL}$  in the constitutive equations should be replaced by  $\overline{\Gamma}_{KL}$ , with equations (46*a*), (47*a*), (48*a*), (49*a*), (50*a*), (51*a*), (52*b*), (53*b*), (54*b*), (55*b*), (56*b*) and (57*b*) being further reduced to

$$T_{11a} = a_2 + a_3 \Gamma_{22} + a_6 \Gamma_{33} + 2a_7 (\Gamma_{11} + \Gamma_{22}), \tag{59}$$

$$T_{22a} = a_2 + a_3 \bar{\Gamma}_{11} + a_6 \bar{\Gamma}_{33} + 2a_7 (\bar{\Gamma}_{11} + \bar{\Gamma}_{22}), \tag{60}$$

$$T_{33a} = a_1 + 2a_5\bar{\Gamma}_{33} + a_6(\bar{\Gamma}_{11} + \bar{\Gamma}_{22}), \tag{61}$$

$$T_{23a} = a_4 \bar{\Gamma}_{23}, \tag{62}$$

$$T_{31a} = a_4 \bar{\Gamma}_{31}, \tag{63}$$

$$T_{12a} = -a_3 \bar{\Gamma}_{12}, \tag{64}$$

$$\Pi_{1d} = -d_1\Gamma_{31} - 2d_{12}(\Gamma_{22}E_1 - \Gamma_{12}E_2) - 2d_{13}\Gamma_{33}E_1 - 2d_{14}(\bar{\Gamma}_{11} + \bar{\Gamma}_{22})E_1 - d_{15}\bar{\Gamma}_{31}E_3,$$
(65)

$$\Pi_{2d} = -d_1 \bar{\Gamma}_{23} - 2d_{12} (-\bar{\Gamma}_{12} E_1 + \bar{\Gamma}_{11} E_2) - 2d_{13} \bar{\Gamma}_{33} E_2 - 2d_{14} (\bar{\Gamma}_{11} + \tilde{\Gamma}_{22}) E_2 - d_{15} \bar{\Gamma}_{23} E_3,$$
(66)

$$\Pi_{3d} = -d_2\bar{\Gamma}_{33} - d_3(\bar{\Gamma}_{11} + \bar{\Gamma}_{22}) - d_{15}(\bar{\Gamma}_{31}E_1 + \bar{\Gamma}_{23}E_2) - 2d_{16}\bar{\Gamma}_{33}E_3 - 2d_{17}(\bar{\Gamma}_{11} + \bar{\Gamma}_{22})E_3,$$
(67)

$$M_{1s} = -s_1 \bar{\Gamma}_{31} - 2s_{12} (\Gamma_{22} B_1 - \Gamma_{12} B_2) - 2s_{13} \Gamma_{33} B_1 - 2s_{14} (\Gamma_{11} + \Gamma_{22}) B_1 - s_{15} \Gamma_{31} B_3,$$
(68)

$$M_{2s} = -s_1 \bar{\Gamma}_{23} - 2s_{12} (\bar{\Gamma}_{11} B_2 - \bar{\Gamma}_{12} B_1) - 2s_{13} \bar{\Gamma}_{33} B_2 - 2s_{14} (\bar{\Gamma}_{11} + \bar{\Gamma}_{22}) B_2 - s_{15} \bar{\Gamma}_{23} B_3,$$
(69)

$$M_{3s} = -s_2 \bar{\Gamma}_{33} - s_3 (\bar{\Gamma}_{11} + \bar{\Gamma}_{22}) - s_{15} (\bar{\Gamma}_{31} B_1 + \bar{\Gamma}_{23} B_2) - 2s_{16} \bar{\Gamma}_{33} B_3 - 2s_{17} (\bar{\Gamma}_{11} + \bar{\Gamma}_{22}) B_3.$$
(70)

### **5.** Small deformation and weak magnetic and electric fields (linear constitutive relations)

If we further assume that the magnetic and electric fields are also weak, then all the quadratic terms with respect to  $E_K$ and  $B_K$  as well as  $\overline{\Gamma}_{KL}$  can also be dropped. Therefore, the corresponding constitutive relations in the case of small deformation and weak magnetic and electric fields are linear, and they can be expressed as

$$T_{11} = a_2 + 2a_7\bar{\Gamma}_{11} + (a_3 + 2a_7)\bar{\Gamma}_{22} + a_6\bar{\Gamma}_{33} + d_3E_3 + s_3B_3,$$

$$(71)$$

$$T_{22} = a_2 + (a_3 + 2a_7)\bar{\Gamma}_{11} + 2a_7\bar{\Gamma}_{22} + a_6\bar{\Gamma}_{33} + d_3E_3 + s_3B_3,$$

$$(72)$$

$$T_{33} = a_1 + 2a_5\bar{\Gamma}_{33} + a_6(\bar{\Gamma}_{11} + \bar{\Gamma}_{22}) + d_2E_3 + s_2B_3,$$

$$(73)$$

$$T_{23} = a_4 \bar{\Gamma}_{23} + 0.5 d_1 E_2 + 0.5 s_1 B_2, \tag{74}$$

$$T_{31} = a_4 \bar{\Gamma}_{31} + 0.5 d_1 E_1 + 0.5 s_1 B_1, \tag{75}$$

$$T_{12} = -a_3 \bar{\Gamma}_{12}, \tag{76}$$

$$\Pi_1 = -d_1 \bar{\Gamma}_{31} - 2b_2 E_1 - f_1 B_1, \tag{77}$$

$$\Pi_2 = -d_1 \bar{\Gamma}_{23} - 2b_2 E_2 - f_1 B_2, \tag{78}$$

$$\Pi_3 = -b_1 - d_2 \bar{\Gamma}_{33} - d_3 (\bar{\Gamma}_{11} + \bar{\Gamma}_{22}) - 2b_3 E_3 - f_2 B_3,$$
(79)

$$M_1 = -s_1 \bar{\Gamma}_{31} - f_1 E_1 - 2c_2 B_1, \tag{80}$$

$$M_2 = -s_1 \bar{\Gamma}_{23} - f_1 E_2 - 2c_2 B_2, \tag{81}$$

$$M_3 = -c_1 - s_2 \bar{\Gamma}_{33} - s_3 (\bar{\Gamma}_{11} + \bar{\Gamma}_{22}) - f_2 E_3 - 2c_3 B_3.$$
(82)

We note that, regardless of the initial stresses, initial polarization and magnetization, there are, in fact, only 17 independent material coefficients,  $a_3$ ,  $a_4$ ,  $a_5$ ,  $a_6$ ,  $a_7$ ,  $b_2$ ,  $b_3$ ,  $c_2$ ,  $c_3$ ,  $d_1$ ,  $d_2$ ,  $d_3$ ,  $s_1$ ,  $s_2$ ,  $s_3$ ,  $f_1$  and  $f_2$  for the corresponding linear materials.

Equations (71)–(82) can be compared to the corresponding linear constitutive relations in the more conventional form characterized by matrices (e.g., Lee and Ma 2007):

$$\begin{cases} T_{11}^{T_{11}} \\ T_{22}^{T_{33}} \\ T_{33}^{T_{31}} \\ T_{12}^{T_{23}} \end{cases} = \begin{bmatrix} c_{11} & c_{12} & c_{13} & 0 & 0 & 0 \\ c_{13} & c_{13} & c_{33} & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & c_{44} & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & c_{66} \end{bmatrix} \begin{bmatrix} \bar{\Gamma}_{11} \\ \bar{\Gamma}_{22} \\ \bar{\Gamma}_{33} \\ 2\bar{\Gamma}_{23} \\ 2\bar{\Gamma}_{31} \\ 2\bar{\Gamma}_{12} \end{bmatrix} \\ + \begin{bmatrix} 0 & 0 & e_{31} \\ 0 & 0 & e_{33} \\ 0 & e_{15} & 0 \\ e_{15} & 0 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix} \begin{cases} -E_1 \\ -E_2 \\ -E_3 \end{cases} \\ \begin{bmatrix} -E_1 \\ -E_2 \\ -E_3 \end{bmatrix} \\ + \begin{bmatrix} 0 & 0 & q_{31} \\ 0 & 0 & q_{33} \\ 0 & q_{15} & 0 \\ q_{15} & 0 & 0 \\ q_{15} & 0 & 0 \\ q_{15} & 0 & 0 \\ e_{31} & e_{31} & e_{33} & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} \bar{\Gamma}_{11} \\ \bar{\Gamma}_{22} \\ -E_3 \\ -B_3 \end{bmatrix},$$
(83)
$$\begin{cases} \prod_{12} \\ \prod_{2} \\ \prod_{3} \\ \end{bmatrix} = \begin{bmatrix} 0 & 0 & 0 & 0 & e_{15} & 0 \\ 0 & 0 & 0 & e_{15} & 0 \\ 0 & 0 & 0 & e_{15} & 0 \\ e_{31} & e_{31} & e_{33} & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} \bar{\Gamma}_{11} \\ \bar{\Gamma}_{22} \\ \bar{\Gamma}_{33} \\ 2\bar{\Gamma}_{23} \\ 2\bar{\Gamma}_{31} \\ 2\bar{\Gamma}_{12} \end{bmatrix} \\ - \begin{bmatrix} k_{11} & 0 & 0 \\ 0 & k_{11} & 0 \\ 0 & 0 & k_{33} \\ - \begin{bmatrix} \alpha_{11} & 0 & 0 \\ 0 & 0 & \alpha_{33} \\ q_{31} & q_{31} & q_{33} & 0 & 0 \\ q_{31} & q_{31} & q_{33} & 0 & 0 \\ q_{31} & q_{31} & q_{33} \\ -E_1 \\ -E_2 \\ -B_3 \end{bmatrix},$$
(84)
$$\begin{cases} M_1 \\ M_2 \\ M_3 \\ M_3 \\ \end{bmatrix} = \begin{bmatrix} 0 & 0 & 0 & 0 & q_{15} & 0 \\ 0 & \alpha_{11} & 0 \\ 0 & \alpha_{11} & 0 \\ 0 & 0 & \alpha_{33} \\ \end{bmatrix} \begin{cases} -E_1 \\ -E_2 \\ -E_3 \\ -E_1 \\ -E_2 \\ -E_3 \\ -E_3 \\ -E_3 \\ \end{bmatrix}$$

 $\begin{bmatrix} \mu_{11} & 0 & 0 \\ 0 & \mu_{11} & 0 \end{bmatrix} \begin{bmatrix} -B_1 \\ -B_2 \\ B_2 \end{bmatrix}.$ 

(85)

From such a comparison, one immediately identifies

$$a_3 = c_{12} - c_{11} = -2c_{66},$$
  $a_4 = 2c_{44},$   $a_5 = \frac{1}{2}c_{33},$   
 $a_6 = c_{13},$   $a_7 = \frac{1}{2}c_{11},$ 

$$b_2 = -\frac{1}{2}k_{11}, \qquad b_3 = -\frac{1}{2}k_{33}, \qquad (86b)$$

$$c_2 = -\frac{1}{2}\mu_{11}, \qquad c_3 = -\frac{1}{2}\mu_{33}, \qquad (86c)$$

 $d_1 = -2e_{15}, \qquad d_2 = -e_{33}, \qquad d_3 = -e_{31}, \quad (86d)$ 

$$s_1 = -2q_{15}, \qquad s_2 = -q_{33}, \qquad s_3 = -q_{31}, \quad (86e)$$

$$f_1 = -\alpha_{11}, \qquad f_2 = -\alpha_{33}. \tag{86} f$$

#### 6. Conclusions

In this paper, we have derived the three-dimensional and fully coupled constitutive equations for a second-order nonlinear transversely isotropic (i.e., 6mm) magnetic crystal. They are expressed in terms of independent material coefficients which need to be determined experimentally or via ab initio calculation or through both approaches. As an application, the constitutive relations for the special case of small deformations together with different magnetic and electric fields are also presented, and the material coefficients corresponding to small deformation and weak magnetic and electric fields can be related to those in the standard linear theory (e.g., Lee and Ma 2007). The present work forms the basis for future nonlinear analysis of dynamically loaded structures composed of magnetoelectroelastic materials with the symmetry class 6mm based on a numerical method (i.e., finite element formation).

#### Acknowledgments

The authors would like to thank the Editor and the reviewers for their constructive comments. Partial support from the Natural Science Fund of China (10772123) and AFRL/ARL are also acknowledged.

#### References

- Aboudi J 2001 Micromechanical analysis of fully coupled electro-magneto-thermo-elastic multiphase composites *Smart Mater. Struct.* **10** 867–77
- Alshits V I, Darinskii A N and Lothe J 1992 On the existence of surface waves in half-infinite anisotropic elastic media with piezoelectric and piezomagnetic properties *Wave Motion* **16** 265–83
- Avellaneda M and Harshe G 1994 Magnetoelectric effect in piezoelectric/magnetostrictive multilayer (2-2) composite J. Intell. Mater. Syst. Struct. 5 501–13
- Benveniste Y and Milton G W 2003 New exact results for the effective electric, elastic, piezoelectric and other properties of composite ellipsoid assemblages J. Mech. Phys. Solids 51 1773–813
- Bichurin M I, Petrov V M, Ryabkov O V, Averkin S V and Srinivasan G 2005 Theory of magnetoelectric effects at magnetoacoustic resonance in single-crystal ferromagnetic–ferroelectric heterostructures *Phys. Rev.* B **72** 060408(R)

- Bustamante R, Dorfmann A and Ogden R W 2008 Nonlinear electroelastostatics: a variational framework Z. Angew. Math. Phys. at press
- Chen J Y, Pan E and Chen H L 2007 Wave propagation in magneto-electro-elastic multilayered plates *Int. J. Solids Struct.* 44 1073–85
- Chen P J, Davison L and McCarthy M F 1976 Electrical responses of nonlinear piezoelectric materials to plane waves of uniaxial strain: application to quartz gauges J. Appl. Phys. **47** 4759–64
- Chung M Y and Ting T C T 1995 The Green function for a piezoelectric piezomagnetic magnetoelectric anisotropic elastic medium with an elliptic hole or rigid inclusion *Phil. Mag. Lett.* **72** 405–510
- Davison L and Graham R A 1979 Shock compression of solids *Phys. Rep.* **55** 255–379 (Review Section of Physics Letters)
- Dorfmann A and Ogden R W 2004 Nonlinear magnetoelastic deformations Q. J. Mech. Appl. Math. 57 599–622
- Dorfmann A and Ogden R W 2005 Nonlinear electroelasticity Acta Mech. 174 167–83
- Du J K, Shen Y P, Ye D Y and Yue F R 2004 Scattering of anti-plane shear waves by a partially debonded magneto-electro-elastic circular cylindrical inhomogeneity *Int. J. Eng. Sci.* **42** 887–913
- Feng W J and Su R K L 2006 Internal crack problem of a functionally graded magneto-electro-elastic strip Int. J. Solids Struct. 43 5196–216
- Feng W J, Su R K L and Liu Y Q 2006 Scattering of SH waves by an arc-shaped interface crack between a cylindrical magneto-electro-elastic inclusion and matrix with the symmetry of 6 mm Acta Mech. 183 81–102
- Feng W J, Xue Y and Zou Z Z 2005 Crack growth of interface crack between two dissimilar magneto-electro-elastic materials under anti-plane mechanical and in-plane electric magnetic impact *Theor. Appl. Fract. Mech.* **43** 376–94
- Feynman R P, Leighton R B and Sands M 1964 *The Feynman* Lectures on Physics vol 2 (Reading, MA: Addison Wesley)
- Fiebig M 2005 Revival of the magnetoelectric effect J. Phys. D: Appl. Phys. **38** R123–52
- Gao C F, Kessler H and Balke H 2003a Crack problem in magnetoelectroelastic solids. Part I: Exact solution of a crack *Int. J. Eng. Sci.* **41** 969–81
- Gao C F, Tong P and Zhang T Y 2003b Interfacial crack problems in magnetoelectroelastic solids Int. J. Eng. Sci. 41 2105–21
- Harshe G, Dougherty J P and Newnham R E 1993 Theoretical modeling of multilayer magnetoelectric composites *Int. J. Appl. Electromagn. Mater.* **4** 145–59
- Hu K Q, Li G Q and Zhong Z 2006 Fracture of a rectangular piezoelectromagnetic body *Mech. Res. Commun.* **33** 482–92
- Jordan N F and Eringen A C 1964 On the static nonlinear theory of electromagnetic thermoelastic solids—I Int. J. Eng. Sci. 2 59–95
- Kankanala S V and Triantafyllidis N 2004 On finitely strained magnetorheological elastomers J. Mech. Phys. Solids 52 2869–908
- Kiral E and Eringen A C 1990 Constitutive Equations of Nonlinear Electromagnetic–Elastic Crystals (New York: Springer)
- Kirchner H O K and Alshits V I 1996 Elastically anisotropic angularly inhomogeneous media II: the green's function for piezoelectric, piezomagnetic and magnetoelectric media *Phil. Mag.* A 74 861–85
- Lee J M and Ma C C 2007 Analytical full-field solutions of a magnetoelectroelastic layered half-plane *J. Appl. Phys.* **101** 083502
- Li J Y 2002 Magnetoelectric Green's functions and their application to the inclusion and inhomogeneity problems *Int. J. Solids Struct.* **39** 4201–13
- Li J Y 2003 Uniqueness and reciprocity theorems for linear thermo-electro-magneto-elasticity *Q. J. Mech. Appl. Mathe.* **56** 35–43
- Li J Y and Dunn M L 1998 Micromechanics of magnetoelectroelastic composites: average fields and effective behavior J. Intell. Mater. Syst. Struct. **9** 404–16

- Lin Y H, Cai N, Zhai J Y, Liu G and Nan C W 2005 Giant magnetoelectric effect in multiferroic laminated composites *Phys. Rev. B* 72 012405
- Liu J X, Fang D N and Liu X L 2007 A shear horizontal surface wave in magnetoelectric materials *IEEE Trans. Ultrason. Ferroelectr. Freq. Control* **54** 1287–9
- Lysne P C 1972 One-dimensional theory of polarization by shock waves: application to quartz gauges J. Appl. Phys. 43 425–31
- Nan C W, Bichurin M I, Dong S X, Viehland D and Srinivasan G 2008 Multiferroic magnetoelectric composites: historical perspective, status, and future directions *J. Appl. Phys.* 103 031101 (Applied Physics Reviews—Focused Review)
- Nan C W, Liu G, Lin Y H and Chen H 2005 Magnetic-field-induced electric polarization in multiferroic nanostructures *Phys. Rev. Lett.* 94 197203
- Pan E 2001 Exact Solution for simply supported and multilayered magneto-electro-elastic plates *J. Appl. Mech.* **68** 608–18
- Pan E 2002 Three-dimensional Green's function in anisotropic magneto-electro-elastic bimaterials Z. Angew. Math. Phys. 53 815–38
- Pan E and Heyliger P R 2002 Free vibrations of simply supported and multilayered magneto-electro-elastic plates *J. Sound Vib.* **252** 429–42
- Pao Y H 1978 Electromagnetic forces in deformable continua Mechanics Today vol IV, ed S Nemat-Nasser (Oxford: Pergamon) pp 209–306
- Soh A K and Liu J X 2005 On the constitutive equations of magnetoelectroelastic solids J. Intell. Mater. Syst. Struct. 16 597–602
- Soh A K, Liu J X and Hoon K H 2003 Three-dimensional Green's functions for transversely isotropic magnetoelectroelastic solids *Int. J. Non-linear Sci. Numer. Simul.* 4 139–48
- Song Z F and Sih G C 2003 Crack initiation behavior in magnetoelectroelastic composite under in-plane deformation *Theor. Appl. Fract. Mech.* **39** 189–207
- Spyropoulos C P, Sih G C and Song Z F 2003 Magnetoelectroelastic composite with poling parallel to plane of line crack under out-of-plane deformation *Theor. Appl. Fract. Mech.* **40** 281–9

- Srinivasan G, Rasmussen E T, Levin B J and Hayes R 2002 Magnetoelectric effects in bilayers and multilayers of magnetostrictive and piezoelectric perovskite oxides *Phys. Rev.* B 65 134402
- Steigmann D J 2004 Equilibrium theory for magnetic elastomers and magnetoelastic membranes Int. J. Non-Linear Mech. 39 1193–216
- Steigmann D J 2008 On the formulation of balance laws for electromagnetic continua *Mathe. Mech. Solids* at press
- Suo Z, Zhao X and Greene W H 2008 A nonlinear field theory of deformable dielectrics J. Mech. Phys. Solids **56** 467–86
- Van den Boomgaard J, Terrell D R, Born R A J and Giller H F J I 1974 An *in situ* grown eutectic magnetoelectric composite material: part 1: composition and unidirectional solidification *J. Mater. Sci.* **9** 1705–9
- Van Run A M J G, Terrell D R and Scholing J H 1974 An *in situ* grown eutectic magnetoelectric composite material: part 2: physical properties *J. Mater. Sci.* 9 1710–4
- Van Suchtelen J 1972 Product properties: a new application of composite materials *Philips Res. Rep.* 27 28–37
- Wang B L and Mai Y W 2007 Applicability of the crack-face electromagnetic boundary conditions for fracture of magnetoelectroelastic materials *Int. J. Solids Struct.* 44 387–98
- Wang J G, Chen L F and Fang S S 2003 State vector approach to analysis of multilayered magneto-electro-elastic plates *Int. J. Solids Struct.* 40 1669–80
- Wang X and Shen Y P 2002 The general solution of three-dimensional problems in magnetoelectroelastic media Int. J. Eng. Sci. 40 1069–80
- Wang X and Zhong Z 2003 A circular tube or bar of cylindrically anisotropic magnetoelectroelastic material under pressuring loading *Int. J. Eng. Sci.* **41** 2143–59
- Yang J S and Betra R C 1995 A second-order theory for piezoelectric materials J. Acoust. Soc. Am. 97 280–8
- Zheng H *et al* 2004 Multiferroic BaTiO<sub>3</sub>–CoFe<sub>2</sub>O<sub>4</sub> nanostructures *Science* **303** 6661–3
- Zhou Z G, Wu L Z and Wang B 2005 The dynamic behavior of two collinear interface cracks in magneto-electro-elastic materials *Eur. J. Mech.* A 24 253–62